CLAY STREET

Baldwin's Corners Southerly

Montville Twp

118

FIELD BOOK

360

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.
NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tabels see end of book.

Baldwin's Corners Southerly
MONTVILLE TWP.

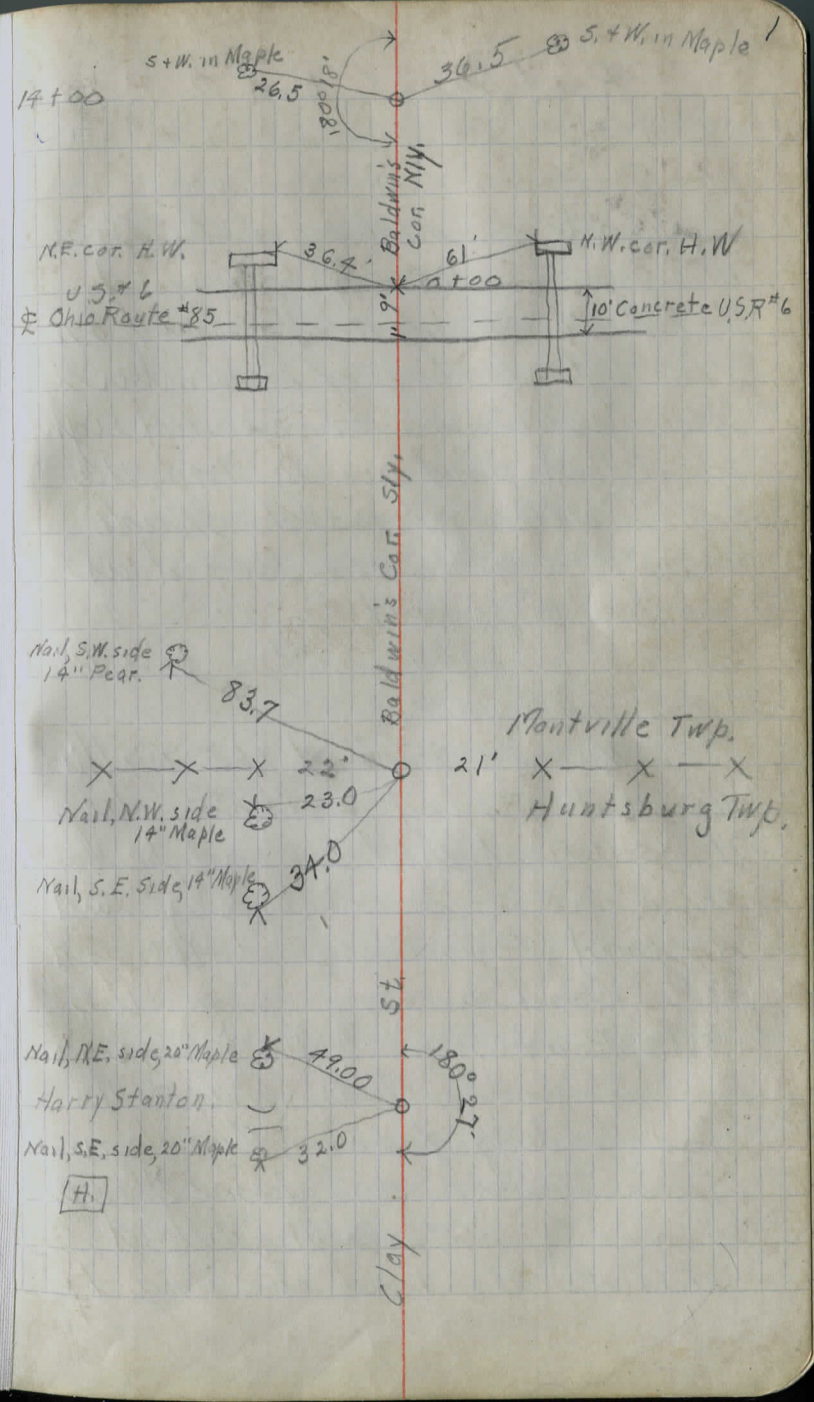
Clay Street - No. 37
Sections - E & F
Align - pg - 1 - 19
X-Sections - pg - 21 - 35
Slope Stakes - pg - 37-51

DRAINAGE COMPLAINT CH 37 G (1981) 72

118

Please return to the
County Surveyor's Office
Chardon Ohio

K. 25-103,
Akron



Road Records, Book B. P. 95

At a meeting of the Board of Commissioners aforesaid held at Chardon aforesaid on the third day of December in the year one thousand eight hundred and twenty two the Committee aforesaid made their Report to the Board as follows to wit -

Geauga County - Montville June 15th 1822

Having Viewed the within described ground we have deemed it expedient that a Road be laid, and have accordingly laid a road beginning on the end of the Road running from the State Road near John Johnson's in Batavia by Reeds Mill to the Road leading from Windsor to Bondstown and from thence running Northwardly till it intersects the Road running by

Mark Burns Esq. in Thompson to the great Road in Madison.

Eben Clark
Shelburn Bostwick } Committee
Dan Miller

"Personally appeared before me Aaron Scott Justice of the Peace for Huntsburg Township. The within named Committee and were duly qualified according to law June 15, 1822 Aaron Scott Justice of the Peace"

"Survey of a Road Beginning at the end of the road running from the state Road near John Johnson's in Batavia by Reeds Mill to the Road leading from Windsor to Bondstown from thence North on the lot line between No 97 & 98 in Huntsburg 20 chs. 10 Ls. to the Townline

Thence Magnetically North 2 miles. N 8° W 2 miles 66 chs 74 Ls. to the North line of Montville

Thence N 18° W 53 chs 69 Ls.

over

to the Road leading by Mark Barris Esq. in Thompson to the great Road in Madison Making in the whole a distance of 5 miles, 60 chains 53 links Claredon November 28th 1822

attest - George E. White
For Rolph Cowles
Surveyor which said Report and survey being publicly read in two different days of the Meeting last aforesaid, and the same being duly examined and fully understood by the Board and no objections being made thereto, and the Board being satisfied that said Road if established will be of public utility it is thereupon ordered by the Board that the same be Established and henceforth taken, deemed and considered as public highway, pursuant to the Statute in such case

made & provided - and that the same be Recorded and opened sixty feet wide.
Attest Eliasee Paine Clerk
of Commissioners

Sept. 11, 1929. Windy, 65°
Marks, Parks, Hassel

TRIAL LINE.

8730) 6.25000 (.00072
61110
13900

.00072
9870
5040
648
648
7.17840

.00072
8560
4320
360
576
6.16320

.00072
9290
6480
144
648
6.68880

.00072
7470
5040
288
504
5,37840

.00072
6430
2160
288
432
4.62960

.00072
3710
720
504
216
2.67120

.00072
2570
5040
360
144
1.85040

1550
.00072
3100
10850
1.11600

99+70

92+90

87+30

85+60 ±

7.4+70 ±

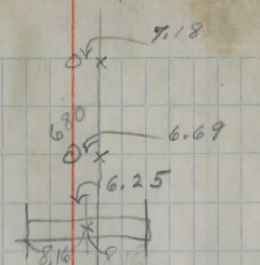
64+30 ±

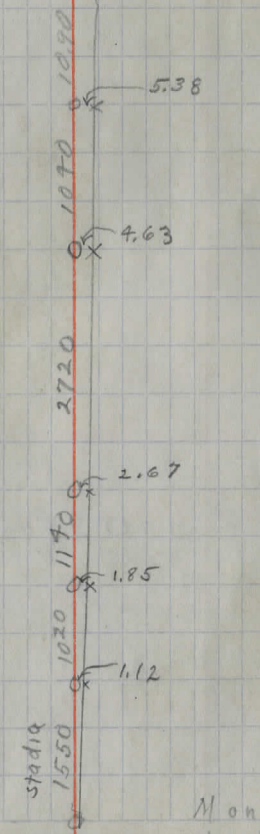
37+10 ±

25+70 ±

15+50 ±

0+00



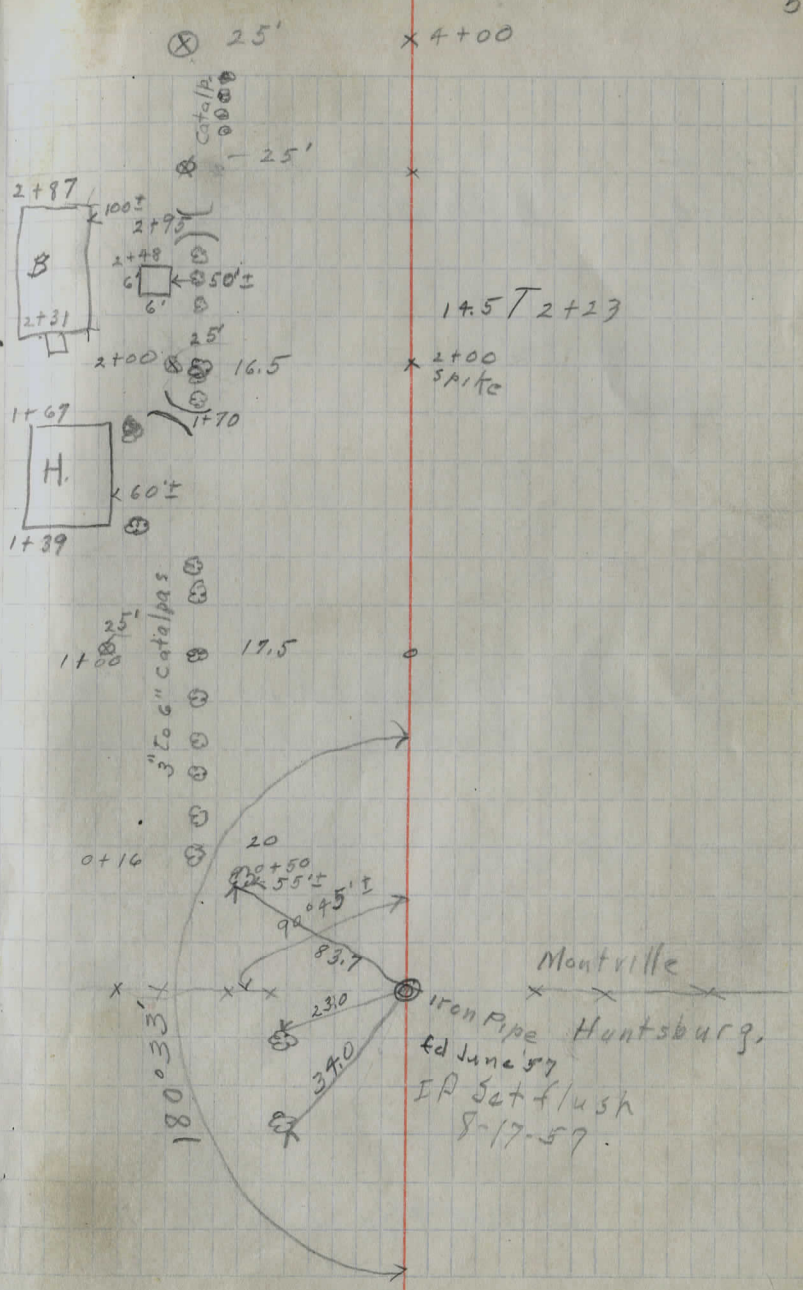


Montr
Hunts

Sept. 12, 1929, Fair, 70°
Marks, Parks, Hassel.

0+00

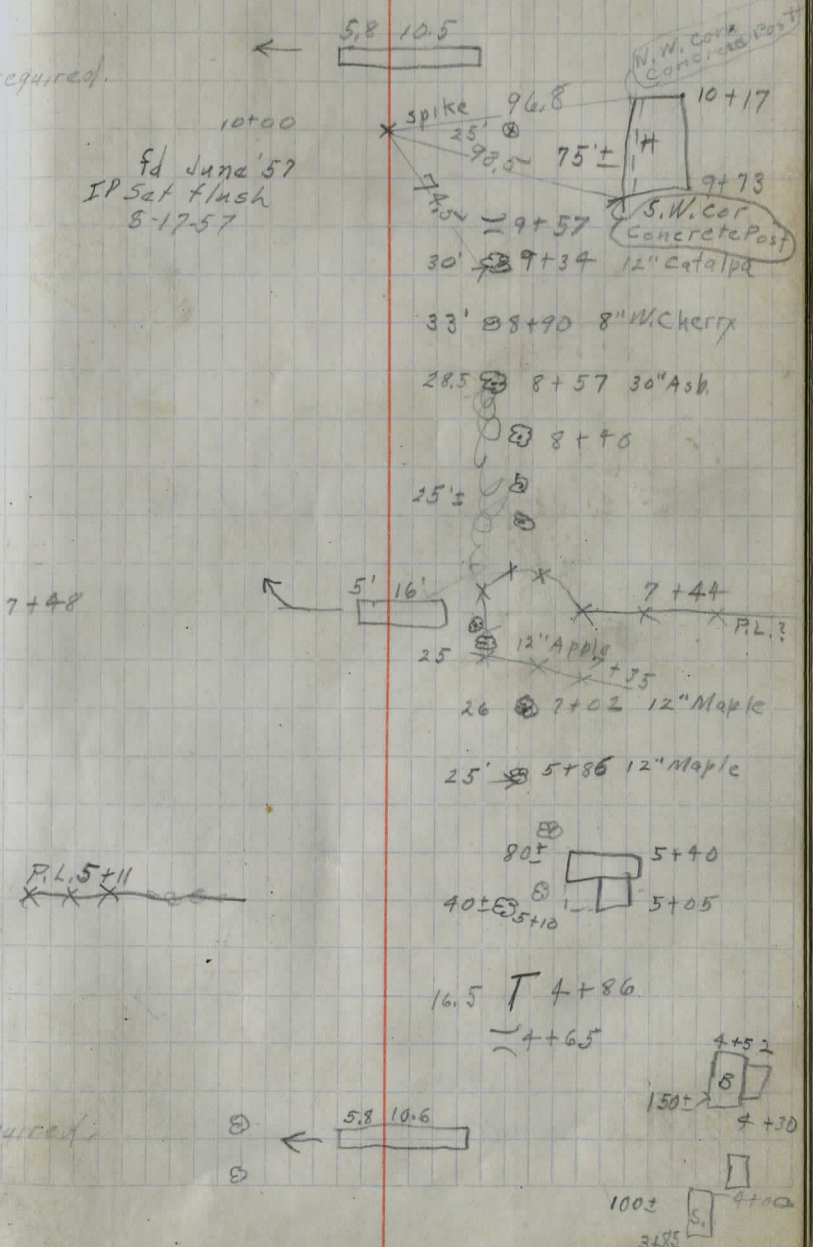
Δ = 0°33' R.



11+34 8" Corr. Pipe 5 acres 15" pipe required.
10+00 Δ = 0°00'

7+48 1½'± x 1'± Stone Culvert, N.G.
15 acres; 18" Pipe required.

4+40 10" Corr Pipe 5 acres 15" Pipe required.

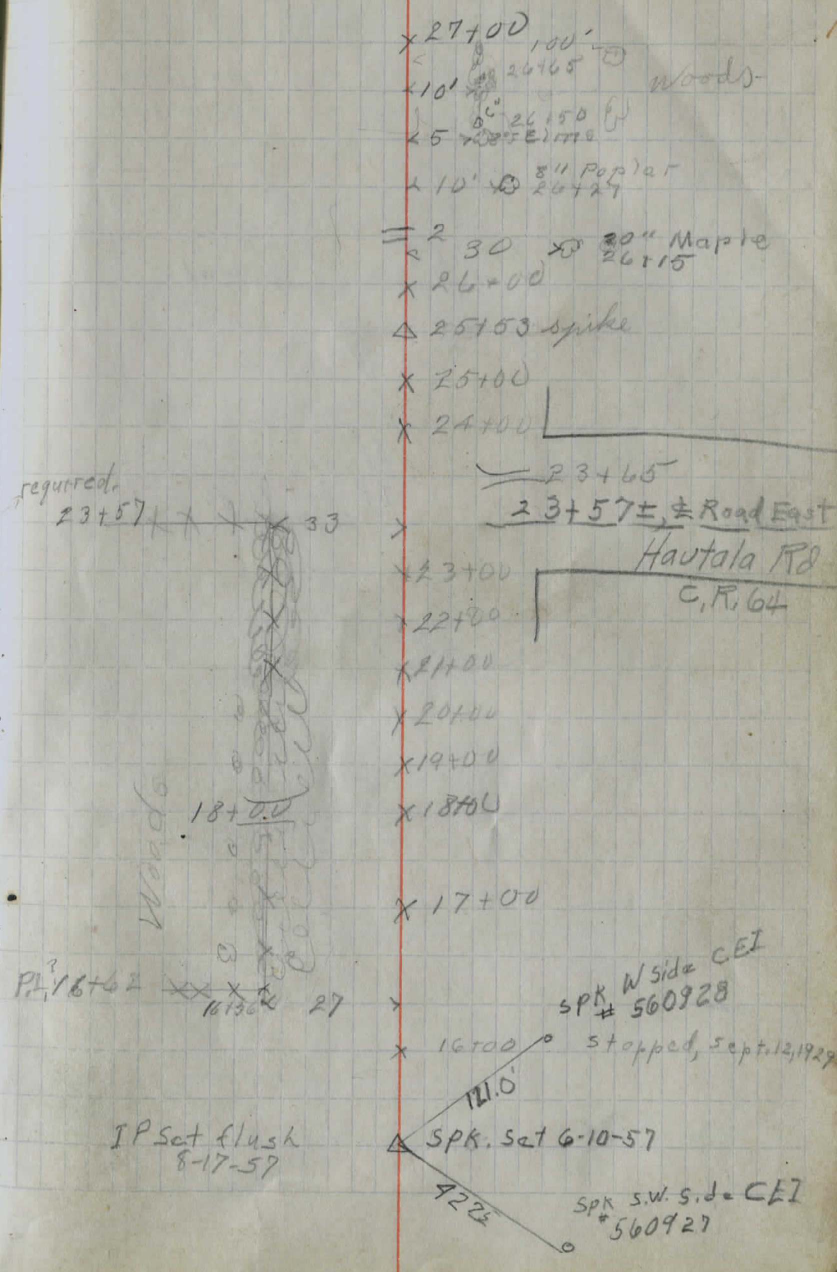


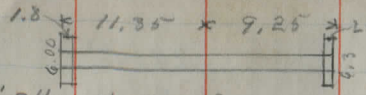
26+20.8 8"x1' ←16.2→ 0.2 old Plank Culvert
25 acres 24" pipe required.

25+53 0°00'

23+57± Side road culvert 10 acres 15" pipe required.

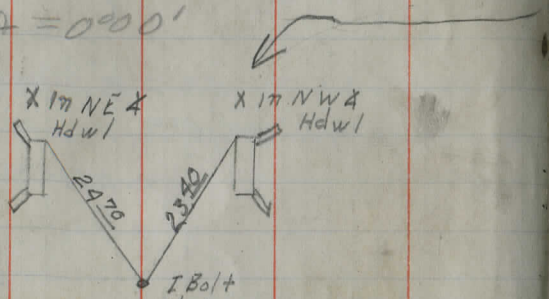
15+43.4 0°00'

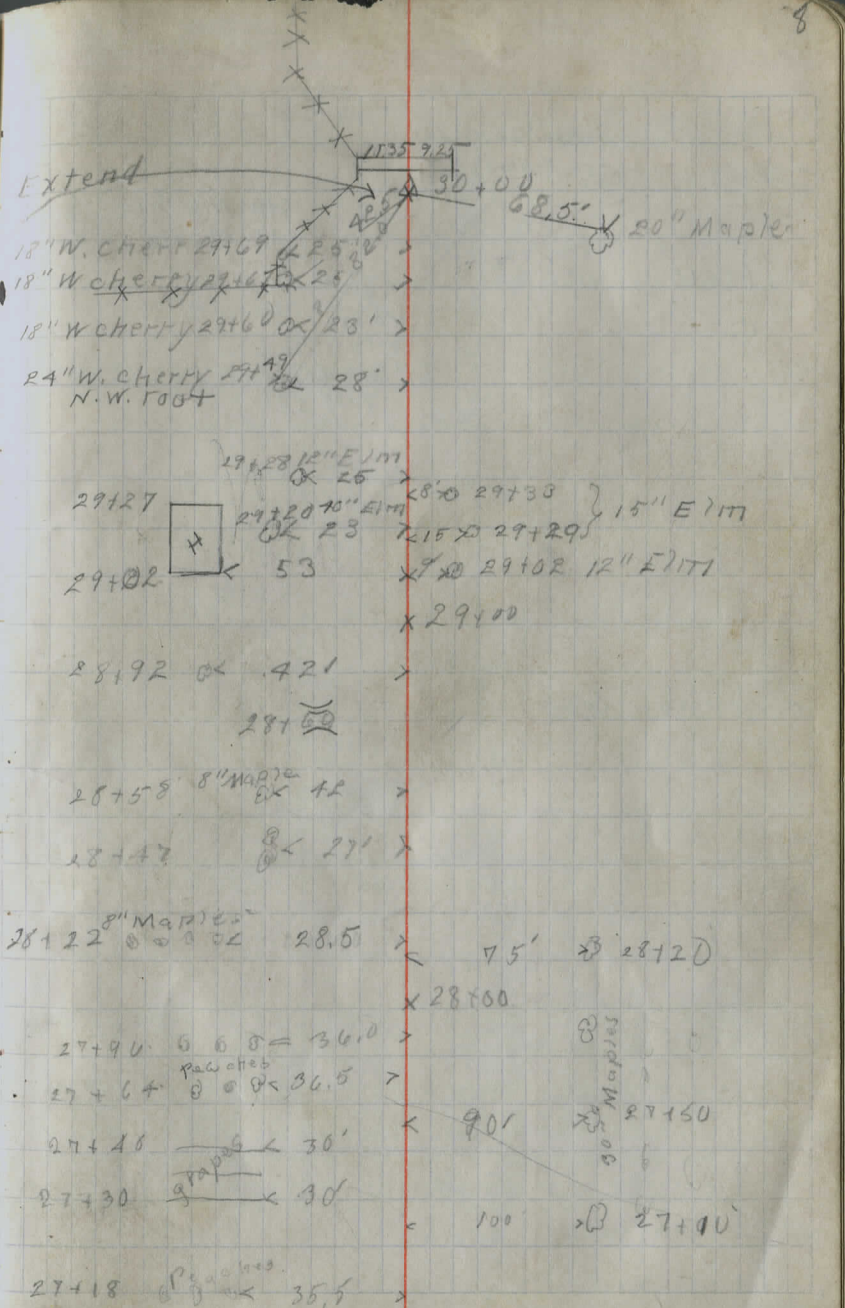


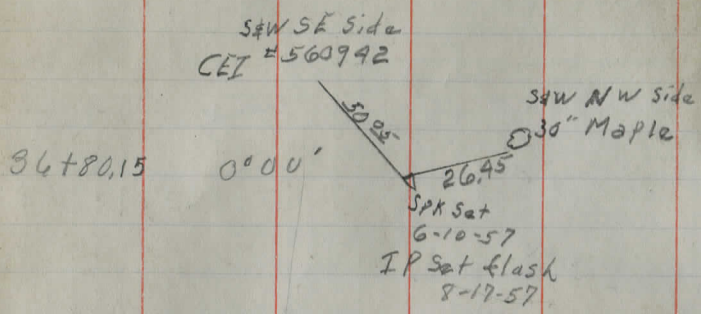


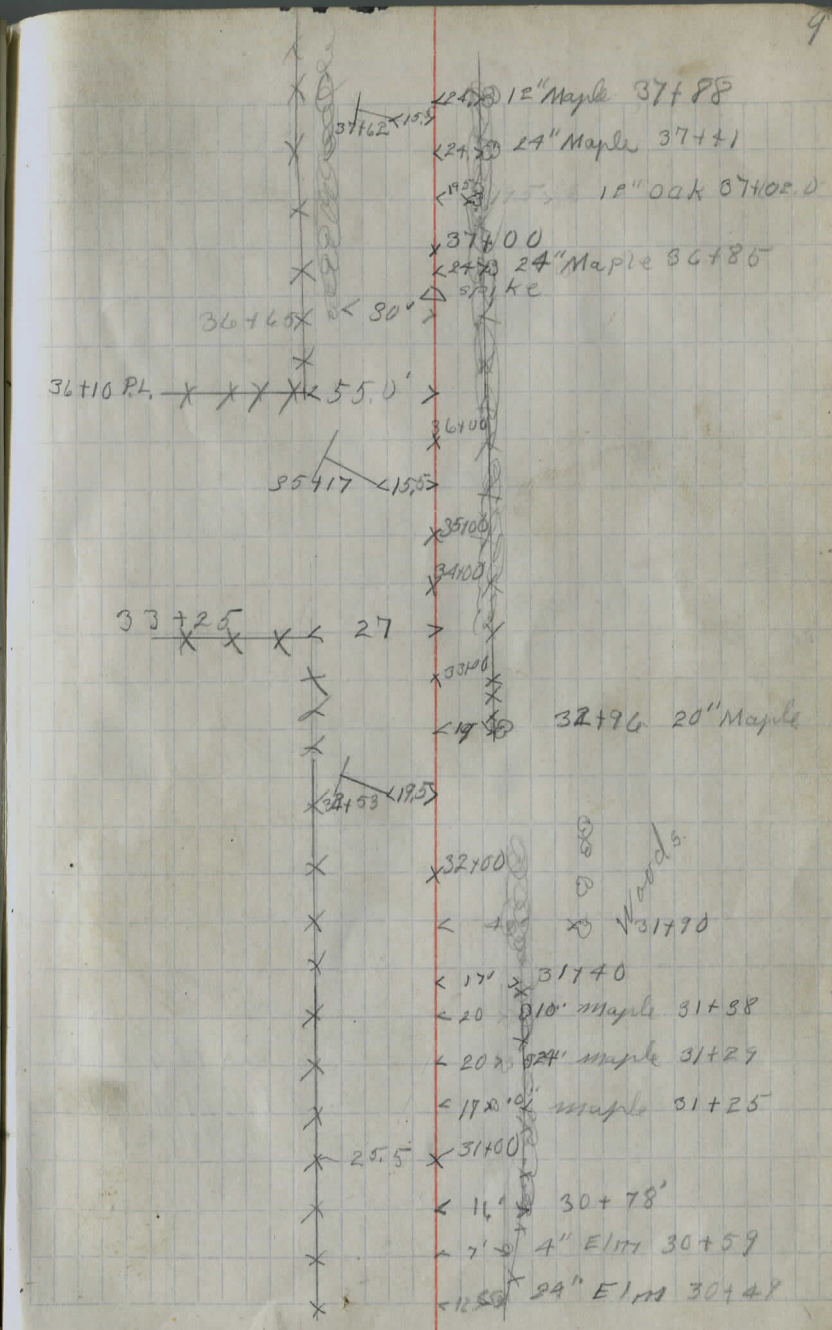
30+15.9 3'8" x 4'2" old stone slab culvert
Fair condition

30+00 Δ = 0°00'






S&W SE Side
CEI ± 560942
50.85'
S&W NW Side
30" Maple
36+80.15
0°00'
26.45'
SPK Set
6-10-57
IP Set Flash
8-17-57

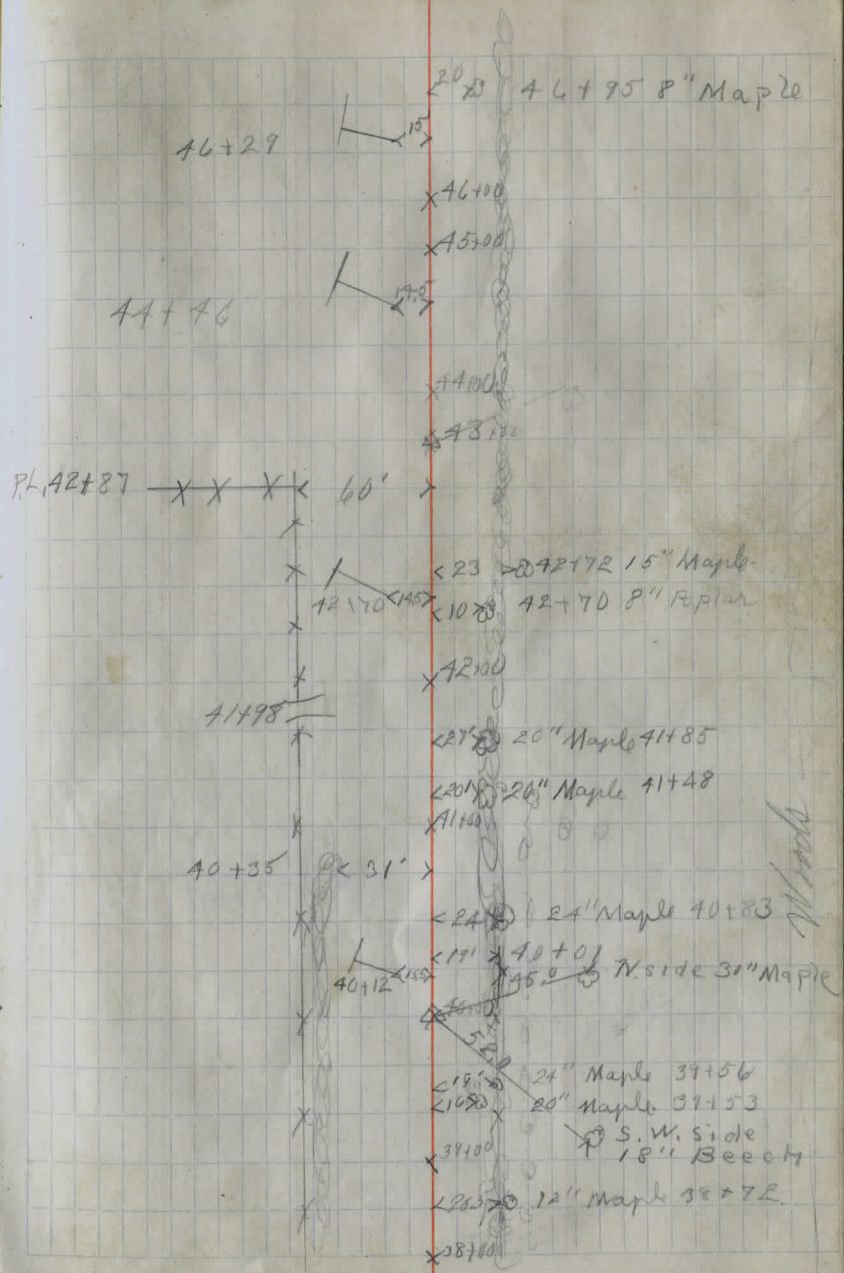

12" Maple 37+88
37+62
15.5'
24" Maple 37+71
12" Oak 37+02.0
37+00
24" Maple 36+85
Stake
36+65
80°
36+10 P.I.
55.0'
36+00
35+17
15.5'
35+00
34+00
33+25
27
33+00
32+96 20" Maple
32+53
19.5'
32+00
Woods
31+90
31+40
20" Maple 31+38
24" Maple 31+27
Maple 31+25
31+00
25.5'
30+78
4" Elm 30+59
24" Elm 30+48

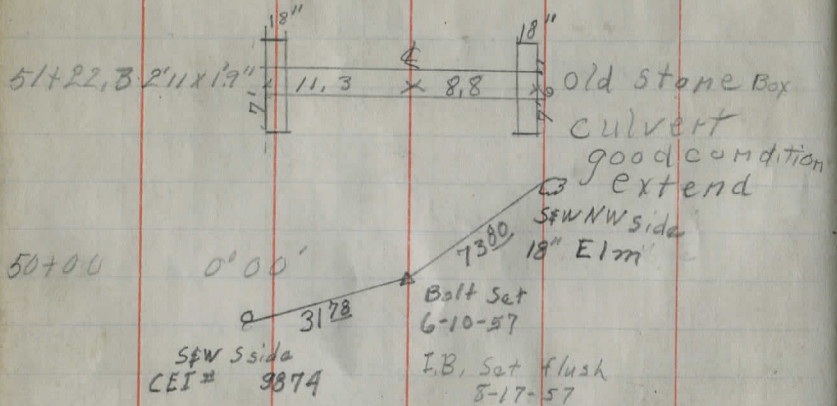
44+50 15" pipe required

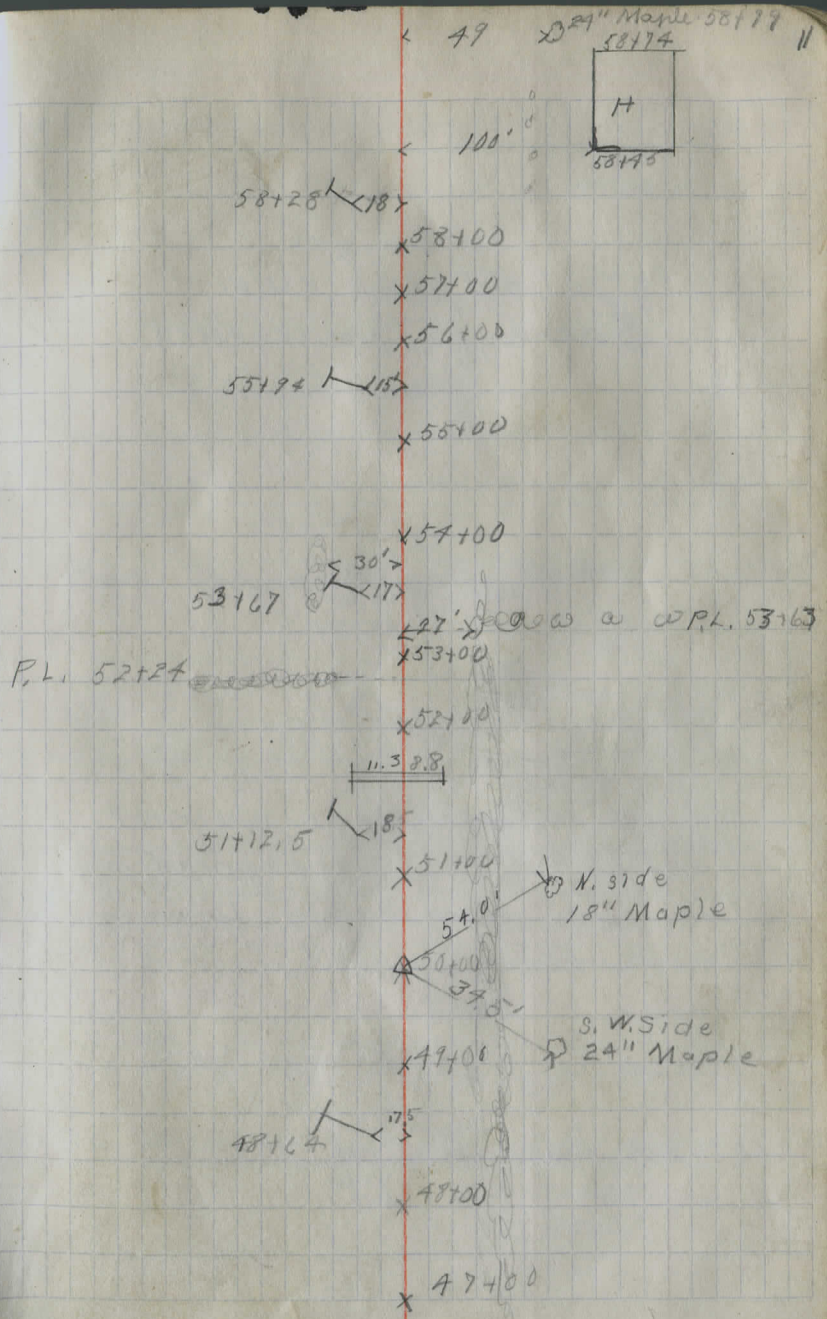
Cool wind 60°
Stopped Sept 16, 1929.
D. Parks
R. Hassel
R. Goodfich

46+00 0°00'

Spk fd 6-10-57
I.P. Sat flash
8-17-57




18"
18"
51+22.8
2'11x1'9"
11.3
8.8
old stone Box culvert
good condition
extend
50+00
0°00'
S&W NW side
18" Elm
73.80
31.78
Bolt Set
6-10-57
S&W S side
CEI # 9874
I.B. Set flush
5-17-57


49
29" Maple 58+77
58+74
H
58+75
100'
58+28
18
58+00
57+00
56+00
55+94
15
55+00
57+00
30'
17
53+67
27'
53+00
P.L. 52+24
52+00
11.3 8.8
18
51+12.5
51+00
54.0'
N. side
18" Maple
50+00
S. W. Side
24" Maple
49+00
48+64
17.5
48+00
47+00

68+76.6 6"x6" old plank culvert
5 acres, 15" pipe required.

65+00 0° 00' Stake —25'— A —25'— Stake
SPK Set
6-10-57

62+38.2 6"x6" old plank culvert
20 acres, 18" pipe required.
61+76 low place natural Drainage

60+00 Stake —25'— A —R5'— Stake
SPK Set
6-10-57

69+62 30" Hickory
36.6
69+08
99 6.3
11' 68+00
67+00
11' 66+20
66+00
65+40 17.6
Tacked Stake 30' 90° 90° 30' Tacked Stake
64+00
63+21 17.6
63+00
10.1 6.8
62+00
11' 61+30 P.L.
61+00
60+80 18'
11' 60+38
Tacked stakes 30' 90° 90° 15' Tacked stake
11' 59+60
59+29
59+00

Cold Cloudy

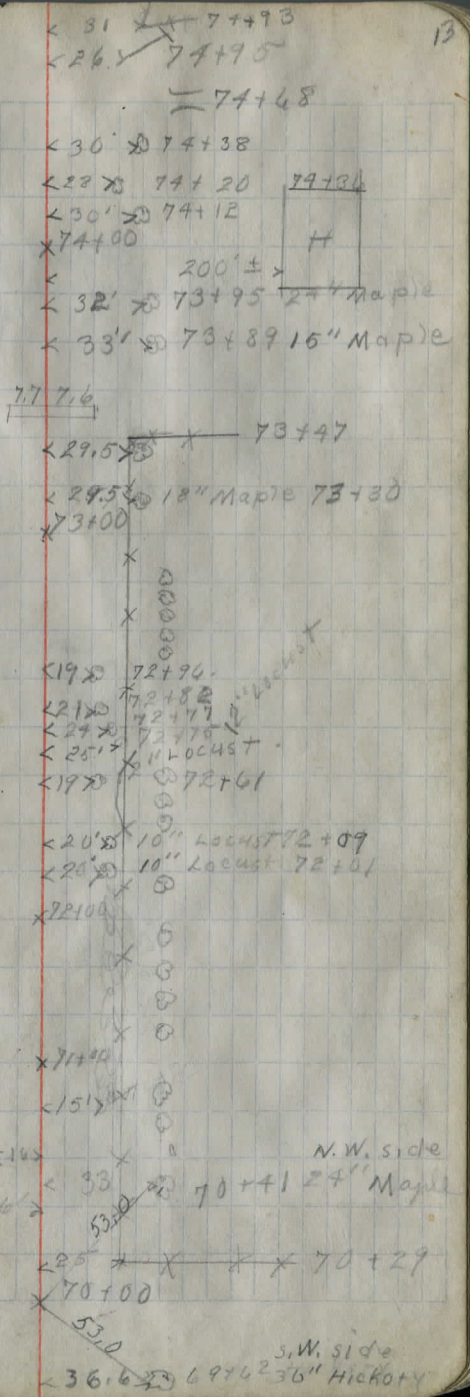
Sept 17, 1929 D. Parks, P. Hassel, R. Goodrich

73+63.9 6"x9" old Wooden Culvert Poor

5 acres, 15" pipe required.

70+06 Δ = 0°00'

Ed 6-11-57
IP Set flush
8-20-57



Sept. 18, 1929, 50° Cloudy, Hail, N. W. Wind.

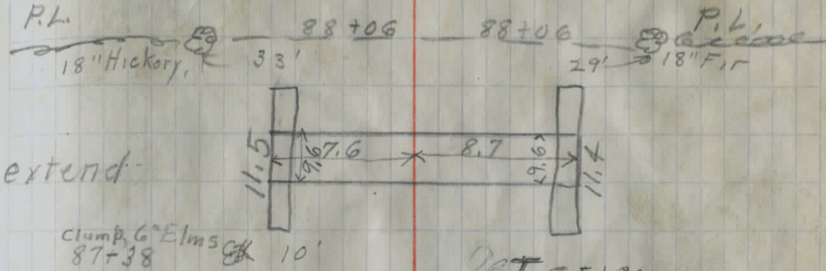
Good Condition

87+52.1 Stone Culvert, Concrete top & H.W.s — extend

82+00 0°00' Stopped Sept. 17, 1929
D. Parks, R.H. Goodrich, R. Hasse)

75+00 Δ 0°00'

23.5 T 88+17



23.5 T 85+96

21.5 T 83+41

Brook

30' tacked stake S.W. side

37.0

28' 81+78 20" Maple

81+00

22 80+88

80+00

27 18" Maple 79+02

79+00

22 78+18

78+00

77+00

76+00

21.5 75+71

22 75+62 15" Maple

75+00

90+00 Δ = 0°00'

96+94

96+64

96+60

B ← 110±

96+20

95+68 24" Maple ⊗ 26.5

95+20

B 110±

94+95

B 110±

94+55

95+20

94+43

G. A. Williams

H ← 70±

94+07

93+58 15" Tree ⊗ 26

93+35 22'

10" Maple 93+17

P.I. 91+61 22.5

10" Maple 91+53 ⊗ 23.5

90+17

H ← 60'±

3" Maple ⊗ 16.5

41.3

10" Maple

89+92

67.3

6" Maple 5

8" Maple 88+44 ⊗ 15.0

88+35

⊗ 96+16, 30" Chestnut

29.5 T 94+53

28 ⊗ 93+60, 18" Maple

28.0 T 92+95

24.5 T 90+74

106 + 66.9, P.T.
106 2° 12'

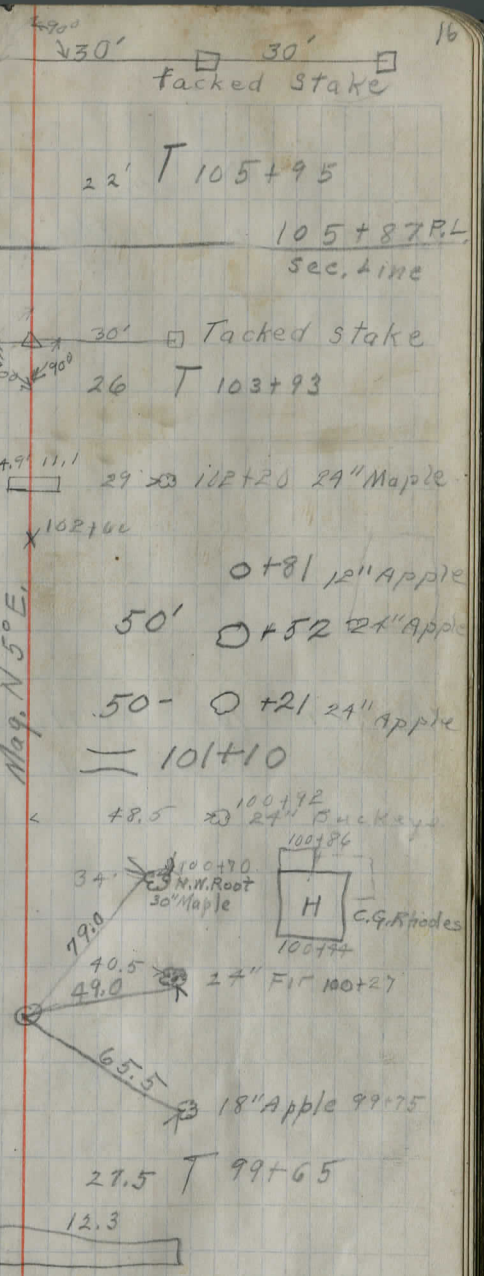
105+90. P.I. Δ = 7°42½ Left,
D = 5°00'
T = 77.3'
L = 154.2

P.C. 105+12.7

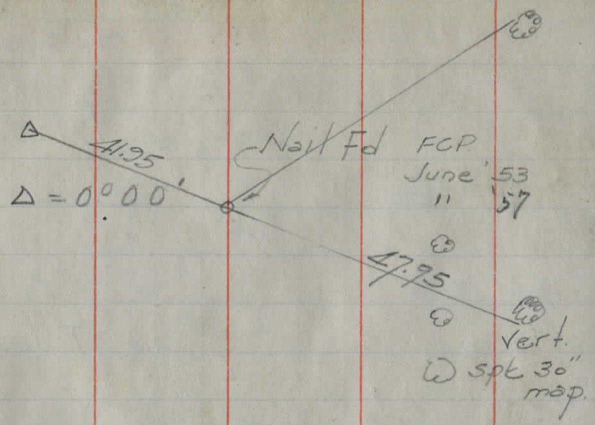
102+20.15 8" Corrugation Pipe culvert
2 acres 15" pipe required

100+00 Δ = 0°00'

97+94, 8" Corr Pipe, fair,
4 acres 15" pipe required,

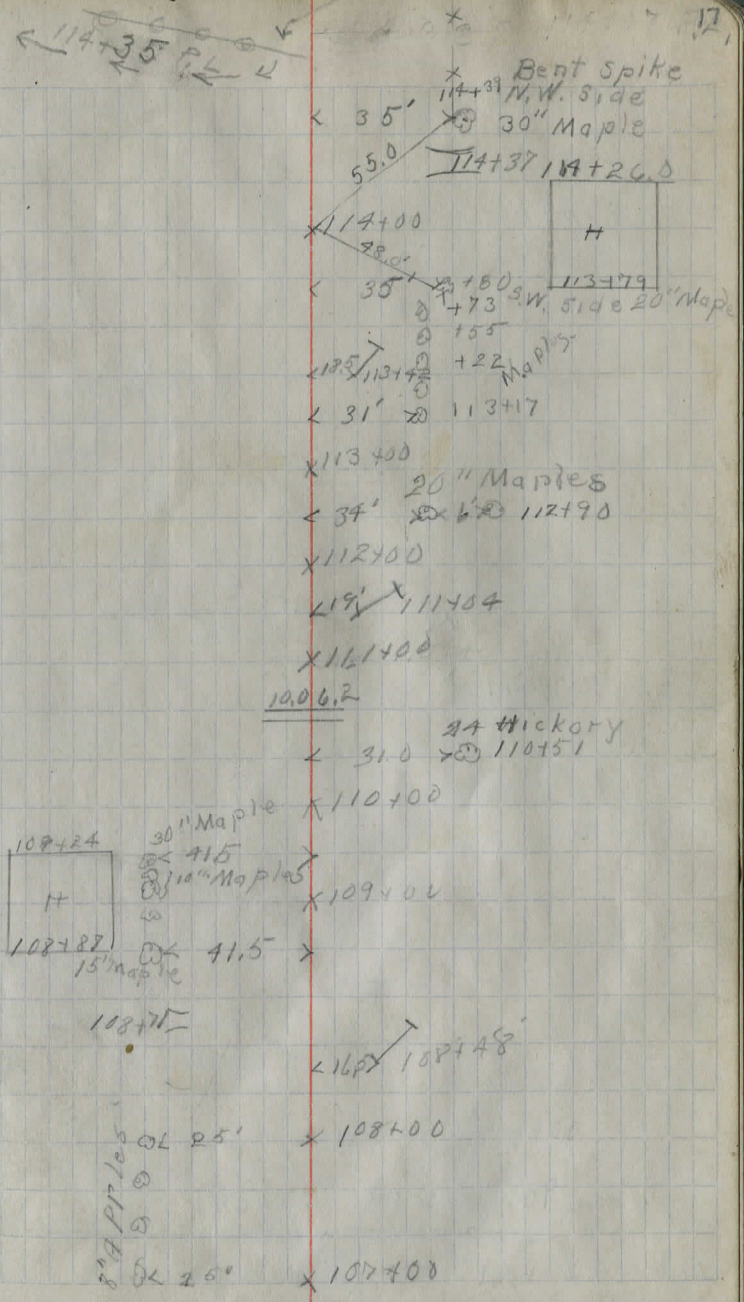


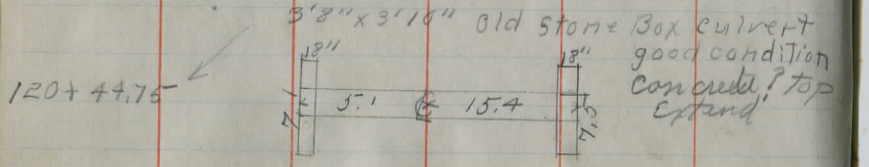
114+00

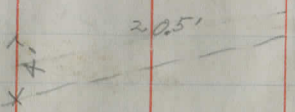


110+98.75 10" corr iron pipe culvert
15 acres 15" pipe required

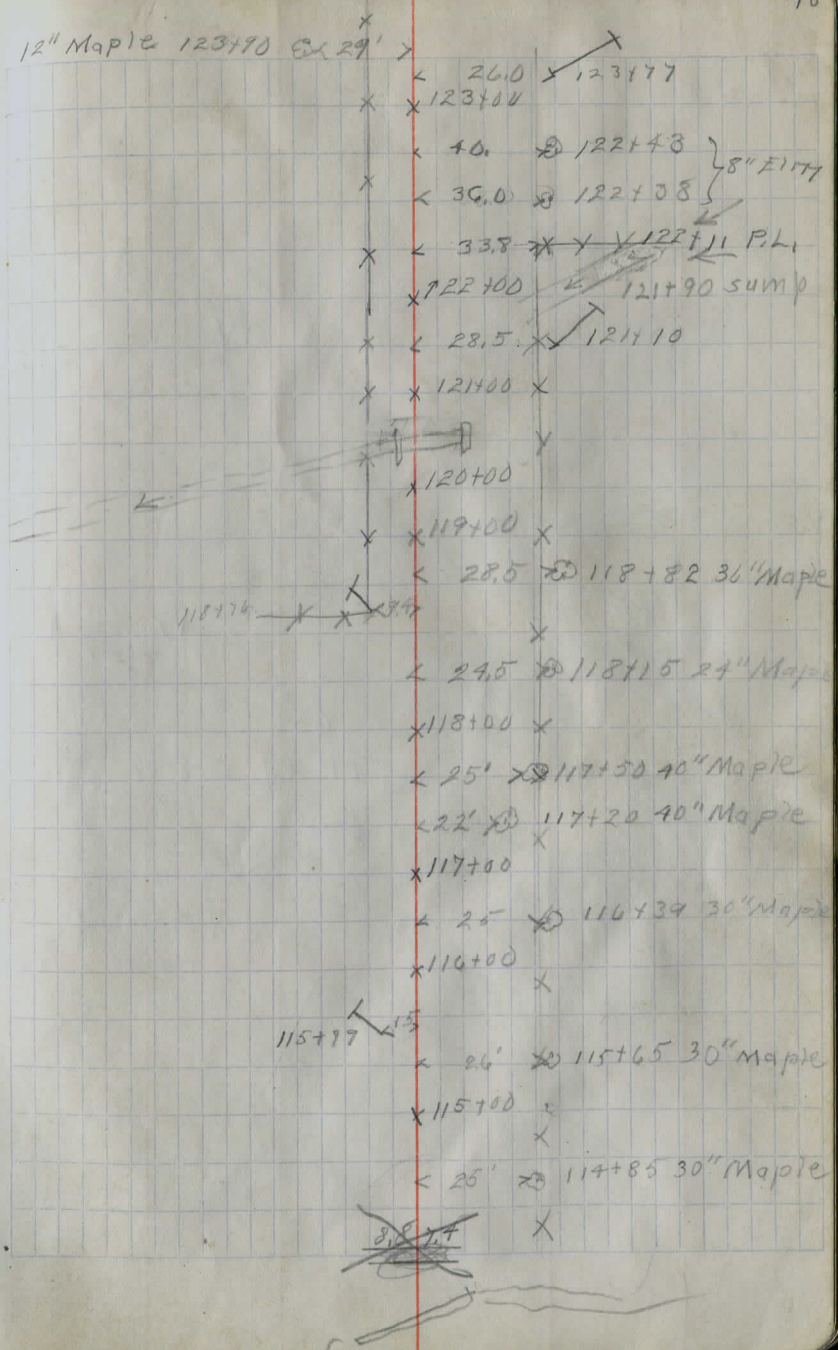
107+00

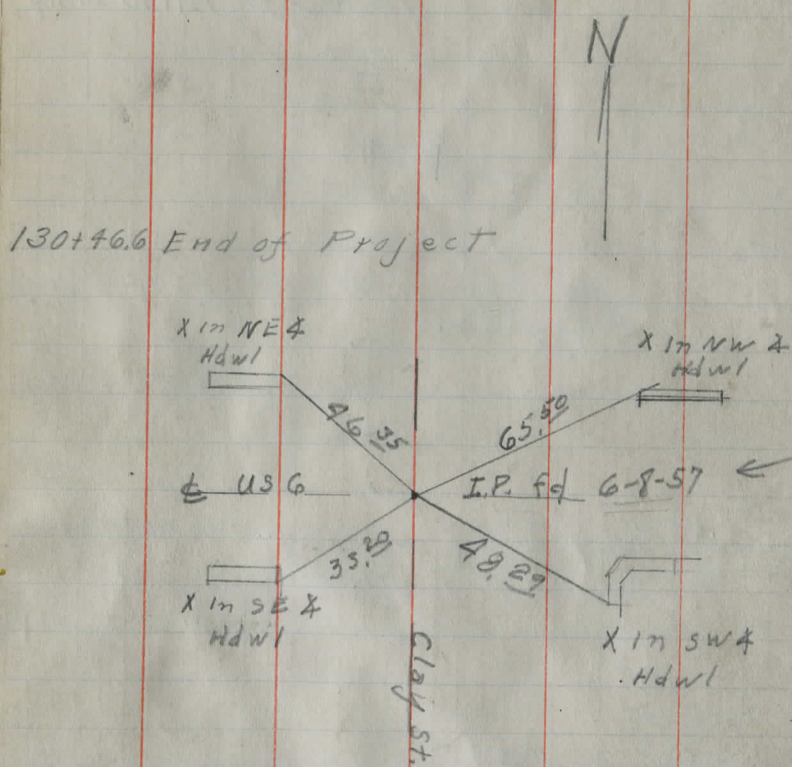


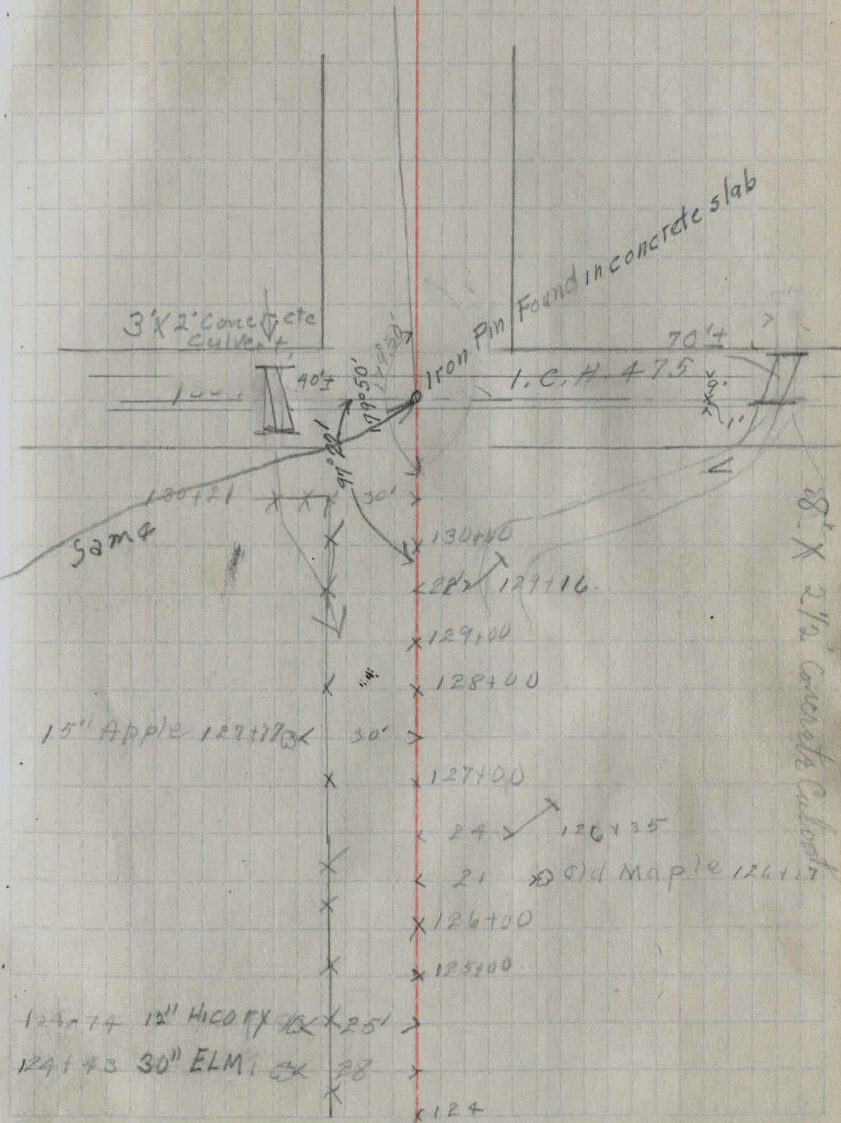




10 Acres Build 15" on skew,
~~Carry water to culvert at 110+98.95~~
114+53.9 10" corr. iron pipe




N
130+46.6 End of Project
X in NE ¼ Hdwl
46.35
X in NW ¼ Hdwl
65.50
℄ US 6
I.P. fd 6-8-57
35.29
48.29
X in SE ¼ Hdwl
X in SW ¼ Hdwl
Clay St.


3'X2' Concrete Culvert
Iron Pin Found in concrete slab
70'±
I.C.H. 475
40'±
179°50'
91°20'
130+21
Same
30'
130+00
22'
129+16
129+00
128+00
15" Apple 127+78
30'
127+00
24
126+35
21
Old Maple 126+17
126+00
125+00
124+74 12" Hicory
25'
124+43 30" ELM
28
124
8' X 2½ Concrete Culvert

Cross Sections

	+	H.I.	−	ELEV.
B.M.				1271.00
	2.42	1273.42		
130+46.4			8.9	1264.5
	3.81	1269.02	8.21	1265.21
130			6.3	1262.7
129			6.4	1262.6
128			6.2	1262.8
T.P.	3.30	1269.65	7.67	1261.35
127			3.3	1261.4
126			4.6	1260.1
125			5.3	1259.4
B.M.			3.94	1260.71

Stopped Sept 19, 1921

D. Parks R, Hassel R, Goodrich

B.M. 4" Ø N.W. Root Maple on Sta. 7+30 of Hamboden-Andover Road.

4.9 / 500.0 — 4.9 / 400.0 — 8.0 / 300 — 8.3 / 200 — 8.6 / 100.0 — 8.7 / ℄

4.5 / ℄ — 4.4 / 100 — 4.3 / 200 — 3.5 / 300 — 2.0 / 400

6.0 / 25.0 — 6.5 / 30.0 — 5.0 / 20.0 — 6.8 / 18.5 — 6.0 / 10.0 — 6.3 / ℄ — 6.0 / 10.5 — 6.0 / 16.5 — 6.4 / 22.5 — 7.5 / 27.0 — 8.0 / 29.5 — 6.2 / ℄ — 35-92

6.8 / 30 — 6.6 / 22.0 — 6.6 / 19.0 — 7.0 / 16.0 — 6.8 / 14.5 — 6.7 / 11.0 — 6.4 / ℄ — 6.6 / 8.5 — 6.3 / 9.0 — 6.3 / 12.5 — 8.2 / 15.0 — 7.9 / 20.0 — 6.8 / 22.0 — 6.2 / 30

6.7 / 30.0 — 6.9 / 24.5 — 6.0 / 19.0 — 7.8 / 15.5 — 8.0 / 13.5 — 7.0 / 10.5 — 6.9 / 8.5 — 6.2 / ℄ — 6.6 / 9.0 — 6.1 / 12.0 — 8.6 / 14.6 — 9.0 / 18.0 — 6.8 / 22.0 — 5.5 / 30.0

3.6 / 30.0 — 3.6 / 18.5 — 4.3 / 15.0 — 4.6 / 12.0 — 3.5 / 8.0 — 4.0 / 7.0 — 3.3 / ℄ — 3.6 / 10.0 — 3.3 / 11.0 — 3.0 / 13.0 — 4.8 / 15.0 — 5.1 / 18.0 — 3.5 / 22.0 — 2.7 / 30.0

3.5 / 30.0 — 3.4 / 25.0 — 4.4 / 21.0 — 6.1 / 18.0 — 6.2 / 16.0 — 4.6 / 13.5 — 4.9 / 12.0 — 4.6 / ℄ — 4.6 / 9.5 — 6.9 / 11.0 — 5.8 / 13.0 — 4.4 / 15.0 — 3.8 / 16.0 — 3.6 / 20.0 — 4.3 / 30.0

4.8 / 30.0 — 4.4 / 17.0 — 6.2 / 13.5 — 6.2 / 11.0 — 5.5 / 9.5 — 5.9 / 8.0 — 5.3 / ℄ — 5.4 / 12.5 — 4.8 / 14.5 — 6.5 / 16.5 — 6.4 / 19.0 — 5.4 / 21.0 — 4.8 / 25.0 — 4.6 / 30

W. Root 30" Elm, 25' Left, Sta. 129 + 43

B.M.	3.11	1263.82		1260.71	W. root 30" Elm, 25' Left Sta. 124+43
124			4.7	1259.1	4.2/30.0 4.8/25.0 4.2/16.0 5.1/14.5 5.6/11.0 4.8/9.5 5.3/7.0 4.7/℄ 5.0/17.5 5.9/18.5 6.0/21.0 5.6/23.0 4.3/30.0
123			4.9	1258.9	5.5/30.0 4.9/14.5 6.1/13.0 6.2/11.0 5.3/10.0 5.4/8.5 4.9/℄ 5.3/14.5 5.4/18.0 6.4/19.0, 21.5 5.6/22.0 5.0/30.0
122			5.1	1258.7	5.6/30.0 5.2/14.5 5.8/13.5 4.0/11.0 5.7/9.5 5.1/℄ 5.3/13.0 4.9/14.5 5.7/17.5 7.0/20.0 4.8/23.0 6.7/24.0 5.7/30.0
121			5.1	1258.7	6.1/30.0 5.5/19.8 5.5/15.0 6.4/13.0 6.3/11.0 6.1/10.0 5.1/5.0 5.1/℄ 5.1/14.0 7.4/20.0 7.2/22.0 5.5/25.0 4.0/34.0
T.P.	4.36	1264.45	3.73	1260.09	
120+44.75 Culvert, inlet runs N+S, || to road, R. Side			4.6	1259.9	1254.9 1255.1 1255.4 1256.4 1255.9 1256.3 1259.0 1261.3 1260.2 1259.9 1260.1 1261.2 1259.1 1255.3 1256.0 1259.7 1260.1 9.4/400 9.4/300 9.1/200 8.1/100 8.6/0.0 8.2 5.5 3.2/5.1 4.3/3.5 4.6/℄ 4.4/14.0 3.3 5.4 9.2/15.4 8.5/21.0 4.8/40.0 5.8/50.0 1253.0 1253.9 1254.2 11.5/700 10.6/600.0 10.3/500
120			5.1	1259.4	6.3/30.00 5.3/6.5 5.6/5.5 5.2/3.5 5.1/℄ 4.6/6.0 5.2/17.0 5.7/18.0 5.8/21.0 4.4/25.0 3.6/30.0
119			4.9	1259.6	4.1/30.0 4.8/9.0 4.7/5.5 5.1/5.0 4.9/℄ 4.5/6.0 5.1/15.5 3.8/19.0 3.5/25.0 3.4/30.0
118			2.8	1261.7	1.6/30.0 2.4/7.0 3.1/6.0 2.9/5.5 2.8/℄ 2.6/9.0 3.2/12.5 1.2/17.0 0.9/25.0 0.6/30.0
T.P.	5.72	1267.62	2.55	1261.90	
117+54			4.7	1262.9	4.7/30.0 4.7/10.0 5.4/7.0 5.2/8.0 4.7/℄ 5.2/10.0 3.4/14.5 2.8/25.0 3.4/30.0
117			5.7	1261.9	5.9/30.0 6.0/9.5 6.2/8.5 6.0/7.0 5.7/℄ 5.9/9.5 6.2/11.0 5.7/11.5 5.2/18.5 4.7/20.0 4.5/25.0, 30.0
116			6.1	1261.5	7.3/30.0 6.6/18.0 6.8/7.5 6.1/℄ 6.5/7.0 6.9/8.5 5.6/13.0 4.7/30.0

		1267.62		
115			7.0	1260.6
T.P.	4.35	1265.23	6.74	1260.88
114+53.9		Culvert, Corr. Iron	4.4	1260.8
114			4.6	1260.6
B.M.			0.56	1264.67
113			5.4	1259.8
112			6.7	1258.5
111			6.7	1258.5
110+98.75			6.8	1258.4
T.P.	7.37	1266.56	6.04	1259.19
110			7.4	1259.2
109			5.4	1261.2
108			4.6	1262.0
107			3.3	1263.3
T.P.	5.81	1271.95	0.42	1266.14

6.4/30.0 6.9/12.0 7.5/10.5 6.8/2.0 7.0/℄ 7.7/8.5 5.9/12.5 5.6/25.0 5.3/30.0

1255.2 1256.0 1257.2 1258.4 1258.9 1259.5 1260.5 1260.8 1260.1 1260.0 1259.1 1259.6 1260.5

10.0/300.0 9.2/250.0 8.0/150.0 6.8/50.0 6.3/F.L. 8.8 5.7 4.7/8.5 4.4/℄ 4.6/6.5 5.2, 4.1/7.4 F.L. 5.6/28.5 4.7/50.0

5.8/30. 5.6/13.5 6.1/12.5 4.8/10.0 4.6/℄ 4.6/9.5 4.9/10.5 4.5/11.5 4.2/15.5 3.2/20.0 2.5/30.0

R.P. Spike S.W. side 20" Maple 35' Rt. Sta 113+80

4.8/30.0 6.1/15.0 6.8/14.0 5.9/12.0 5.7/11.5 5.4/℄ 5.2/8.5 6.0/11.0 5.0/12.0 4.2/15.0 3.0/20.0 2.8/30.0

6.8/30.0 7.1/14.5 7.3/13.5 7.0/12.0 6.5/1.5 6.7/℄ 6.8/8.0 7.7/11.5 7.2/12.5 6.4/30.0

7.8/30.0 6.9/14.5 8.3/12.5 6.8/10.0 6.7/℄ 7.1/5.5 7.8/7.5 7.0/10.0 6.6/30.0

1253.0 1254.0 1255.0 1255.6 1256.8 1257.0 1257.3 1257.9 1258.4 1258.2 1257.4 1257.5 1259.0 1259.5

12.2/300.0 11.2/200.0 10.2/100 9.6/50.0 8.4/[illegible] 8.2/12.5 7.9, 7.3/10.0 4.8/℄ 7.0, 7.8/6.0 F.L. 7.7/9.0 6.2/50.0 5.7/100.0

ditch at 110+50

7.6/30.0 7.1/15.5 7.4/14.5 7.1/13.0 7.2/12.0 7.4/℄ 7.7/6.5 7.2/8.5 7.9/10.0 6.9/11.5 6.1/14.5 4.9/30.0

5.5/30.0 5.6/20.0 5.9/16.5 5.7/13.0 5.2/5.0 5.4/℄ 5.4/5.5 5.6/10.5 6.4/11.5 5.2/12.5 4.6/30.0

6.5/30.0 5.3/13.5 4.7/12.0 4.9/11.5 4.6/℄ 4.5/6.0 4.5/10.0 5.3/11.5 4.7/12.0 4.4/30.0

2.9/30.0 3.4/11.0 3.8/10.0 3.3/℄ 3.7/9.5 3.8/12.5 2.7/15.0 2.3/20.0 2.0/30.0

R.P. Hub 60' Rt. of Sta 106+66.9

		1271.95		
106			6.9	1265.1
105			5.4	1266.6
104			4.2	1267.8
103			5.1	1266.9
102+20.15			5.9	1266.1
	5.94	1272.06	5.83	1266.12
102			5.9	1266.2
101			5.3	1266.8
B.M.			1.25	1270.81
100			4.8	1267.3
99			8.4	1263.7
98			9.4	1262.7
	4.41	1266.87	9.60	1262.46
97+94			4.4	1262.5
97			4.8	1262.1

6.5 6.6 7.1 6.9 6.7 6.8 6.9 6.4 5.4 4.7
30.0 13.0 12.0 ℄ 6.0 9.0 11.0 12.0 20.0 30.0

6.8 5.8 6.0 5.7 5.1 5.5 7.8 4.3
30.0 8.0 6.5 ℄ 12.5 14.0 15.0 30.0

5.5 5.2 4.9 5.2 4.7 4.2 3.7 4.1 3.6 2.8 2.5
30.0 25.0 9.0 7.5 7.0 ℄ 14.5 16.5 17.0 25.0 30.0

4.0 5.6 5.1 4.8 5.2 4.6 3.7 3.1
30.0 7.5 ℄ 12.5 14.5 15.5 17.5 30.0

1257.3 1259.8 1264.8 1265.4 1265.9 1266.1 1266.4 1265.5 1264.9 1265.5
14.7 12.2 7.2 6.6 6.1 5.9 5.6 6.5 7.1 6.5
200.0 100.0 4.7 ℄ 11.5 20.0

8.6 7.4 5.8 6.0 5.9 5.8 6.4 6.3 5.7 5.2 5.0
30.0 12.0 5.5 3.5 ℄ 15.0 15.5 17.5 18.5 20.0 30.0

7.6 6.6 6.9 5.7 5.3 4.8 4.6 4.5
30.0 11.0 9.5 6.0 ℄ 12.0 24.5 30.0

R.P. spike
N.W. root 30" Maple 34' Rt. Sta 100+70

6.9 5.8 5.9 5.3 6.6 4.8 4.9 5.7 5.4 4.5 3.2
30.0 10.5 9.5 5.0 6.5 ℄ 9.0 11.0 13.0 14.5 30.0

5.0 8.3 8.8 8.4 8.2 8.3 8.9 8.3 7.3
30.0 8.5 7.5 ℄ 2.0 11.0 12.5 14.1 30.0

11.3 10.6 10.0 9.6 9.4 9.2 9.3 10.1 9.5 10.1 9.3
30.0 7.0 5.0 4.5 ℄ 7.5 10.5 12.5 13.0 15.5 30.0

1255.5 1257.7 1261.3 1262.2 1262.5 1263.1 1262.3 1261.5 1261.8 1262.9
11.4 9.2 5.6 5.2 4.6 4.4 3.8 4.6 5.4 5.1 4.0
200.0 100.0 10.0 3.5 ℄ 12.3 17 30.0

5.3 4.9 4.8 4.4 4.1 5.0 4.3 4.1 2.8
30.0 6.5 ℄ 9.6 11.5 15.5 17.0 21.5 30.0

		1266.87		
96			5.0	1261.9
95			6.8	1260.1
T.P.	4.25	1263.77	7.35	1259.52
94			4.0	1259.8
93			4.8	1259.0
92			7.6	1256.2
91			8.9	1254.9
T.P	3.26	1258.47	8.56	1255.21
90			4.9	1253.6
89			6.0	1252.5
88			6.7	1251.8
B.M.			7.24	1251.23
T.P.	3.29	1256.90	4.86	1253.61
87+52.1	Culvert		4.3	1252.6
	3.23	1256.84		1253.61
87			4.9	1251.9
T.P	5.74	1258.33	4.25	1252.59
86			5.1	1253.2
T.P.			2.28	1256.05

7.1/30.0 4.2/25.0 6.0/14.0 5.5/7.5 5.0/℄ 5.1/13.0 5.7/15.0 5.2/15.5 4.7/18.5 3.7/21.0 2.4/30.0

7.2/30.0 7.2/7.5 6.8/℄ 6.6/13.0 7.0/14.5 6.3/16.0 6.1/19.5 4.3/23.0 4.0/30.0

5.0/30.0 4.3/9.0 4.0/℄ 3.9/10.5 4.6/13.0 4.5/15.5 4.0/18.0 2.9/22.0 2.6/30.0

5.3/30.0 5.0/12.5 5.6/11.0 5.5/9.0 4.8/℄ 5.1/11.0 6.1/14.5 5.3/15.5 3.0/25.0 2.5/30.0

7.3/30.0 7.4/20 7.5/10.5 7.9/8.6 7.6/℄ 7.7/10.5 8.4/12.5 7.0/19.5 6.6/30.0

9.3/30.0 9.2/9.5 9.5/8.5 8.9/℄ 9.1/11.0 9.6/14.0 8.6/16.5 9.4/30.0 —

5.0/30.0 4.8/10.5 5.1/9.0 4.9/℄ 4.9/10.5 4.7/13.0 5.3/14.0 4.7/15.0 4.2/17.5 4.0/30.0

6.1/30.0 6.2/10.5 6.4/9.0 6.0/℄ 6.1/11.0 6.6/13.0 4.7/14.5 5.3/25.0 4.9/30.0

7.4/30.0 6.7/10.5 6.8/10.0 6.9/8.0 6.7/℄ 6.7/7.5 6.4/9.0 7.3/11.5 7.5/30.0

E. Root 18" Hickory, Left, Sta. ~~86~~ 88+06, 33' from ℄

N.E. corner West Headwall

1249.2 7.7/100 1249.2 7.7/50.0 1249.8 7.1/25.0 1249.0 7.9 1251.5 5.4 1253.6 3.3 /7.6 1252.5 4.4/6.5 1252.6 4.3/℄ 1252.6 4.3/7.5 1253.6 3.3 1251.5 5.4 1248.8 8.1 /8.7 1249.7 7.2/25.0

1248.9 8.0/150.0 1247.9 9.0/200.0

5.7/30.0 4.9/7.0 5.0/6.0 4.9/℄ 5.1/13.0 5.7/16.0 5.8/18.5 4.0/25.0 3.9/30.0

9.6/30.0 5.1/16.5 6.0/12.5 6.1/10.5 5.4/8.0 5.5/7.0 5.1/℄ 5.3/13.5 6.0/17.5 6.2/20.0 4.5/25.0 4.9/30.0

Top of Sta Stake 85

Stopped Sept. 20, 1929 ~~D. Parks~~, D. Parks

Fair Cool Wind R. Goodrich

R. Hassel

	4.29	1260.34		1256.05
85			5.0	1255.3
84			4.7	1255.6
83			4.3	1256.0
	4.79	1260.25	5.08	1255.26
82			4.4	1255.9
81			4.8	1255.5
80			5.0	1255.3
	5.74	1261.46	4.53	1255.72
79			5.7	1255.8
78			5.0	1256.5
77			4.1	1257.4
76			2.4	1259.1
	5.42	1266.45	0.43	1261.03
75			5.5	1261.0
74			4.3	1262.2

Top of Sta stake At 85

5.8/30.0 5.7/14.5 6.8/12.0 5.5/8.5 5.0/E 5.1/13.5 4.3/16.0 4.6/18.5 7.0/20.0 6.8/20.5 5.3/30.0

4.9/30.0 5.2/16.0 5.6/14.5 6.3/12.0 5.1/10.0 4.7/E 4.8/10.5 4.5/11.0 5.6/15.0 6.2/18.5 4.8/30.0

4.7/30.0 4.9/16.0 5.7/13.0 4.8/10.5 4.9/9.5 4.8/E 4.3/10.0 5.3/14.0 5.9/16.0 5.5/17.5 4.3/20.0 3.7/30.0

4.4/30.0 4.8/13.0 5.6/11.5 4.8/9.5 4.7/E 4.6/8.0 4.3/10.0 5.7/12.0 4.2/25.0 3.9/30.0

5.3/30.0 5.1/11.0 5.5/9.5 5.1/8.5 4.8/E 5.0/9.0 5.0/12.0 5.4/14.5 4.5/30.0

5.2/30.0 5.2/15.0 5.1/12.5 4.5/10.5 5.4/9.0 5.2/7.5 5.0/E 5.0/9.5 5.4/11.5 4.9/13.5 5.4/16.0 5.4/17.0 5.1/30.0

6.7/30.0 6.7/17.0 5.7/11.0 6.1/9.5 6.1/8.0 5.7/E 6.1/8.5 5.8/11.5 6.2/13.5 6.1/17.0 5.1/25.0 4.9/30.0

5.9/30.0 5.5/10.0 5.0/E 5.0/9.0 5.7/8.5 11.0 5.3/12.0 5.6/16.5 5.2/30.0

5.3/30.0 4.6/11.0 4.8/9.5 4.3/8.0 4.1/E 4.1/8.0 4.5/9.5 3.8/12.0 3.7/30.0

2.9/30.0 2.7/12.0 3.1/10.0 2.8/9.0 2.4/E 2.8/8.0 2.5/11.0 3.1/12.0 2.7/14.5 0.5/25.0 0.1/27.0 0.3/30.0

7.0/30.0 6.3/11.5 6.2/10.0 5.7/9.0 5.5/E 5.6/8.0 4.6/12.5 5.2/14.5 4.6/16.0 4.8/17.5 4.5/21.0 3.7/25.0 3.5/30.0

6.8/30.0 5.2/9.5 5.3/8.0 4.8/7.5 4.3/E 4.4/9.0 5.1/12.5 4.5/13.5 4.8/16.0 3.9/18.0 2.8/30.0

		1266.45		
73+63.9			4.4	1261.9
73			4.1	1262.4
B.M.			2.42	1264.03
T.P.	7.52	1270.17	3.80	1262.65
72			7.5	1262.7
71			5.4	1264.8
70+60			4.2	1266.0
T.P.	2.30	1270.68	1.79	1268.88
70			5.5	1265.2
69			6.5	1264.2
68+76.4			5.9	1264.8
68			5.5	1265.2
67			3.6	1267.1
	5.21	1271.93	3.96	1266.72
66			5.2	1266.7
65			4.8	1267.1

1256.0 1257.3 1259.3 1260.8 1261.6 1261.8 1261.9 1262.0 1261.9 1261.3 1260.9 1264.1

11.7/300.0 10.5/200.0 9.2/100.0 7.2/50.0 5.7-4.9-4.7 F.L. 7.7 4.6/2 4.6 4.6 5.3 F.L. 7.6 5.6/11.0 2.7/50

5.7/30.0 5.5/15.0 4.9/10.0 5.0/5.0 4.1/2 4.4/7.0 5.1/9.5 4.3/11.5 4.4/12.5 2.8/25.0 2.6/30.0

S.W. Root 24" Maple 32' Rt. Sta. 78+95

9.9/30.0 9.5/17.0 8.6/11.5 8.6/10.0 8.1/8.0 7.5/2 7.9/6.0 8.7/9.0 8.2/10.0 7.6/25.0 7.5/30.0

5.3/30.0 5.8/13.5 6.6/11.0 5.9/10.0 5.4/2 5.9/7.0 6.2/8.0 5.2/10.0 2.7/14.0 2.6/30.0

7.3/30.0 6.8/25.0 6.3/13.0 6.4/11.5 6.1/10.5 5.5/2 5.5/7.0 5.1/8.0 4.9/10.0 3.6/30.0

8.0/30.0 7.8/18.0 6.9/12.5 7.0/11.0 6.5/8.5 6.5/2 4.3/4.5 5.9/7.0 4.8/9.5 6.2/12.0 5.3/30.0

1268.1 1257.3 1260.1 1263.5 1264.7 1265.0 1264.8 1264.8 1264.6 1263.9 1264.5

12.6/300.0 11.4/200.0 9.8/100.0 7.2 F.L. 9.9 - 6.0 5.7 5.9/2 5.9-6.1-6.8 6.3 3.2/50.0

5.8/30.0 5.7/24.5 5.9/13.0 6.8/11.5 5.9/10.0 6.5/2 5.8/4.0 5.3/7.5 5.6/8.5 4.3/30.0

4.4/30.0 4.4/14.0 4.0/12.0 3.4/5.0 3.6/2 3.7/4.0 2.7/6.0 3.6/7.5 3.1/13.0 2.3/30.0

6.2/30.0 5.5/14.5 5.7/14.0 5.1/5.5 5.2/2 5.0/2.5 5.4/6.0 4.7/8.5 3.9/30.0

4.6/30.0 4.9/17.5 5.5/14.5 5.0/13.5 4.6/6.0 4.8/2 4.8/3.5 5.0/6.0 5.6/7.5 4.9/10.0 4.0/30.0

		1271.93		
64			5.8	1266.1
63			8.1	1263.8
	5.44	1268.66	8.71	1263.22
62+38.2	E. end covered.		5.4	1263.3
62			5.5	1263.2
61.776	Natural drainage		5.6	1263.1
61			5.2	1263.5
60+30			4.0	1264.7
	2.28	1266.74	4.20	1264.46
60			3.1	1263.6
59			5.8	1260.9
	4.29	1268.75		1264.46
B.M.			1.58	1267.17

Fair warm Stopped Sept 21 1929
P. Parks, R. Goodrich, R. Hassel

5.1 5.6 6.4 5.8 5.6 6.0 5.7 5.2 4.2
30.0 13.0 11.0 4 6.0 7.5 9.0 12.0 30.0

9.8 8.8 8.3 8.6 8.4 8.1 7.9 8.3 8.1 8.5 8.1 8.4 7.8
30.0 14.5 13.0 12.0 10.5 4 4.0 6.0 7.5 9.0 10.5 11.5 30.0

1258.0 1258.8 1260.6 1261.8 1263.3 1263.6 1264.6
10.7 9.9 8.1 6.7 5.7 5.4 4.1
300.0 200.0 100.0 70.1 4 6.8 P.T. 50.0

6.7 5.9 6.5 5.8 5.5 5.9 6.1 5.8 6.2 5.5 5.0
30.0 15.0 13.0 10.5 4 6.5 7.0 8.0 10.5 13.0 30.0

1257.7 1258.9 1260.3 1261.0 1261.7 1262.2 1263.1 1262.6 1263.1 1263.1 1264.2
11.0 9.8 8.4 7.7 7.0 6.5 5.6 6.1 5.6 5.6 4.5
300.0 200. 100.0 50.0 10.5 7.5 4 5.0 7.0 9.0 50.0

6.6 5.8 6.1 5.8 5.1 5.2 5.4 6.1 5.6 5.8 5.9 5.0 4.4
30.0 15.3 13.5 12.0 3.0 4 4.0 6.0 7.5 9.0 15.0 20.0 30.0

4.7 4.1 4.1 4.9 4.0 4.1 4.7 4.4 2.5 1.4 0.8 +0.2
30.0 25.0 13.5 11.5 4 6.0 8.0 9.0 13.0 16.0 18.0 30.0

2.9 2.7 3.7 3.1 3.1 3.6 3.0 0.8 0.1 +0.6
30.0 18.0 14.5 4 3.0 6.0 7.5 13.5 17.0 30.0

6.9 6.6 6.6 7.0 6.2 5.8 5.9 5.6 5.6 2.7
30.0 18.0 16.0 14.5 5.0 4 4.0 4.5 7.5 30.0

W. root 24" Maple 49' Rt. Sta. 58+79

Fair 75° Sept. 23. 1929

D. Parks, R. Goodrich, C. Rand.

B.M.	1.35	1268.52		1267.17
58			9.4	1259.1
	4.04	1262.20	10.36	1258.16
57			4.0	1258.2
56			5.1	1257.1
55			5.1	1257.1
54			6.6	1255.6
	4.23	1258.02	8.41	1253.79
53			4.2	1253.8
52			4.9	1253.1
	2.80	1257.81	3.01	1255.01
51+22.3			4.5	1253.3
51			4.7	1253.1
	5.30	1259.12	3.99	1253.82
50			5.3	1253.8
	1.70	1259.80	4.02	1255.10
49			4.6	1255.2
	5.19	1260.12	4.87	1254.93
48			4.8	1255.3

W. root 24" Maple 49' Rt. Sta. 58+79.

10.7 10.6 9.9 10.1 9.4 9.4 9.8 9.5 8.1
30.0 17.0 15.0 14.0 4 1.5 2.5 4.5 30.0

5.5 4.5 4.8 3.9 4.0 4.0 4.5 3.7 2.6
30.0 13.5 12.5 6.5 4 1.5 3.0 5.0 30.0

6.4 5.0 5.6 5.0 5.1 5.1 5.4 4.8 5.5 4.7
30.0 13.0 11.5 9.5 4 5.0 6.0 8.0 7.5 30.0

5.9 5.8 6.5 5.1 5.0 5.4 5.0 5.6 4.4
30.0 11.0 9.5 4 7.0 4.0 10.0 12.0 30.0

6.8 6.6 7.7 6.6 6.4 6.9 4.6 7.1 5.6
30.0 13.5 10.5 4 7.5 9.5 10.5 12.0 30.0

4.1 3.9 4.6 4.8 4.2 4.6 3.8 4.1 3.5 4.3 4.1 3.2 3.0
30.0 15.0 13.0 11.0 4 4.5 7.0 10.5 13.0 14.0 16.0 17.0 30.0

5.9 4.7 5.3 4.9 4.9 5.4 4.8 4.3 4.8
30.0 13.0 12.5 4 3.5 5.0 6.0 20.0 30.0

1249.7 1250.3 1250.8 1251.5 1250.9 1252.8 1250.0 1253.3 1253.9 1250.0 1252.8 1251.1 1251.9 1252.8
R.I 7.5 7.0 6.3 6.9 5.0 2.8 4.5 7.5 3.9 2.8 5.0 6.7 5.9 5.0
30.0 20.0 20.0 5.0 Rt. 11.8 4.5 4 6.5 5.8 Rt. 50.0 100.0
1249.9 1248.9 1249.1
9.9 8.7 8.7
700 600 500

5.7 5.2 4.7 4.9 5.2 5.2 5.6 5.9
30.0 11.0 4 4.5 6.0 7.5 10.0 30.0

5.1 4.7 5.7 6.4 5.7 5.2 5.3 5.5 6.0 5.5 3.9
30.0 17.0 12.0 12.5 10.0 2.5 4 5.0 7.5 20.0 30.0

5.0 5.0 4.8 5.5 4.6 5.0 6.6 5.3 4.9 4.9
30.0 14.0 12.5 11.5 4 7.5 6.5 7.0 10.0 30.0

6.0 5.0 5.6 4.6 4.8 5.0 5.4 5.1 5.7 5.3
30.0 12.5 11.0 3.5 4 4.5 6.0 7.0 9.0 10.5

5.3 4.1 4.1
12.5 15.5 30.0

		1260.12		
	5.06	1260.92	4.24	1255.86
B.M.	3.29	1260.96	3.25	1257.67
47			4.9	1256.1
46			4.7	1256.3
	5.38	1260.81	5.53	1255.43
45			5.0	1255.8
44			5.0	1255.8
	5.09	1260.98	4.92	1255.89
43			5.1	1255.9
	5.59	1262.62	3.95	1257.03
42			5.6	1257.0
41			4.0	1258.6
	4.71	1264.10	3.23	1259.39
40			4.8	1259.3
39			4.0	1260.1
	3.90	1263.71	4.29	1259.81
38			4.3	1259.4
B.M.			3.49	1260.22

Westroot 24" Maple 40' Rt. Sta. 47+20

6.3 / 30.0	5.4 / 12.5	6.1 / 14.0	5.7 / 12.0	4.9 / 2	5.0 / 3.5	5.7 / 6.0	5.0 / 7.0	5.5 / 9.0	3.6 / 18.0	3.4 / 30
6.2 / 30.0	5.7 / 15.0	6.0 / 13.0	5.1 / 9.0	4.7 / 2	4.9 / 6.5	5.4 / 7.0	4.9 / 8.0	5.5 / 10.0	5.1 / 12.5	4.1 / 30.0
6.5 / 30.0	5.7 / 12.5	5.7 / 10.5	5.6 / 9.0	5.0 / 2	5.1 / 7.5	5.7 / 9.0	5.2 / 10.0	5.6 / 11.5	3.7 / 20.0	3.6 / 30.0
5.9 / 30.0	5.5 / 12.5	5.7 / 11.0	5.3 / 9.0	5.0 / 2	5.1 / 6.0	5.7 / 7.5	5.2 / 9.0	5.6 / 10.0	4.1 / 30.0	
6.2 / 30.0	5.6 / 12.0	5.9 / 11.0	5.5 / 9.0	5.1 / 2	5.1 / 6.0	6.2 / 9.5	6.1 / 30.0			
5.5 / 30.0	5.5 / 10.0	6.0 / 9.0	5.7 / 7.0	5.6 / 2	5.9 / 7.5	5.6 / 9.5	6.0 / 11.5	5.1 / 20.0	5.5 / 30.0	
4.3 / 30.0	4.5 / 13.0	5.0 / 11.0	4.5 / 9.0	4.0 / 2	4.3 / 7.0	4.5 / 8.0	4.3 / 9.5	4.7 / 11.0	3.2 / 30.0	
5.2 / 30.0	5.3 / 14.0	5.9 / 11.5	5.2 / 10.0	4.8 / 2	5.4 / 7.0	4.4 / 30.0				
5.0 / 30.0	5.1 / 14.0	5.5 / 12.5	4.7 / 10.0	4.0 / 2	4.4 / 6.5	4.7 / 8.5	4.3 / 8.5	4.9 / 10.5	3.9 / 30.0	
4.8 / 30.0	5.2 / 14.5	5.7 / 12.5	4.8 / 11.0	4.9 / 9.5	4.3 / 2	4.4 / 6.0	4.8 / 7.0	4.6 / 8.5	5.1 / 11.0	3.9 / 15.0	3.7 / 30.0

W. root 24" Maple 24' Rt. 37+41

		1263.71		
37			5.9	1257.8
	3.75	1261.41	6.05	1257.66
36			4.5	1256.9
35			6.2	1255.2
	4.83	1259.22	7.02	1254.39
34			4.5	1254.7
33			4.8	1254.4
	3.01	1258.40	3.83	1255.39
32			5.4	1253.0
31			10.1	1248.3
	3.08	1253.00	8.48	1249.92
30+15.9			5.0	1248.00
30			5.2	1247.8
B.M.			1.54	1251.46
	6.74	1256.70	3.04	1249.96
29			7.9	1248.8
28			6.0	1250.7

6.2/30.0 6.6/14.0 7.2/12.0 6.3/9.5 5.1/℄ 5.9/6.5 6.2/8.5 6.5/10.5 5.0/30.0

5.4/30.0 4.8/12.8 5.3/10.5 4.7/9.5 4.5/℄ 4.9/6.0 5.2/10.5 4.3/30.0

6.3/30.0 6.1/12.0 6.4/10.5 6.2/℄ 6.2/5.0 5.9/6.0 6.4/8.5 4.8/30.0

5.8/30.0 5.0/13.0 5.3/11.0 4.9/10.0 4.5/℄ 4.8/4.5 5.0/5.5 4.8/7.0 5.2/12.5 4.2/30.0

5.6/30.0 5.4/14.0 5.7/12.5 4.9/10.0 4.8/℄ 4.9/4.0 5.5/5.5 5.3/7.0 5.8/9.0 4.9/30.0

3.8/30 5.6/15.5 6.4/13.5 5.4/11.0 5.4/℄ 5.8/3.5 5.6/5.0 6.3/8.5 4.1/16.0 4.4/30.0

12.2/30.0 10.7/12.5 10.1/11.0 9.8/4.0 10.1/℄ 10.5/3.5 10.6/6.5 9.1/30.0

1242.8 1243.5 1243.9 1243.2 1243.0 1247.2 1249.9 1248.1 1248.00 1248.1 1250.0 1247.2 1243.0 1244.2 1245.0

9.2/00 9.5/200 9.1/100 9.8/50 10.0 5.8 3.1/11.35 4.9/9.0 5.0/℄ 4.9/7.2 3.0 5.8 10.0/9.25 8.8/50 8.0/100

1243.5 1243.7 1242.3 1241.5 1241.4 1241.4 1240.9

9.5/400 9.3/600 10.7/700 11.5/800 11.6/900 11.6/1000 12.1/1100

7.5/30.0 6.4/11.5 5.3/8.0 5.2/℄ 5.2/3.5 4.8/5.0 4.1/10.0 8.4/30.0

N. W. root 24" W Cherry 28' Lt Sta. 29+49

5.7/30.0 8.2/8.5 7.7/2.5 7.9/℄ 8.0/2.5 8.6/4.5 8.0/6.5 9.1/17.0 9.4/30.0

4.3/30.0 5.1/17.0 6.3/14.5 6.2/11.0 5.7/5.0 6.0/℄ 6.1/3.5 6.7/4.0 5.9/7.0 7.0/25.0 7.8/30.0

Fair 80' Sept 24, 1929
D. Parks, R. Goodrich, C. Rand

		1256.70		
27			5.1	1251.6
			5.5	1251.2
26+20.8			~~6.6~~	~~1250.1~~
26			5.2	1251.5
	7.16	1259.12	4.74	1251.96
25			7.2	1251.8
24			6.2	1252.9
23			5.0	1254.1
22			3.8	1255.3
	7.21	1264.61	1.72	1257.40
21			7.2	1257.4
20			5.7	1258.9
19			3.7	1260.9
18			0.8	1263.8
	14.18	1277.93	0.86	1263.75
17+40			11.3	1266.6
17			9.0	1268.9

3.8 4.2 5.1 5.2 5.1 5.2 5.7 5.5 5.2 5.9
30.0 20.0 11.5 7.5 ℄ 3.5 4.0 7.0 25.0 30.0

1250.6 1250.3 1250.4 1250.2 1251.2 1251.0 1250.1 1249.9 1249.7 1248.6 1247.7
5.9 6.1 6.4 6.3 4.5 3.5 5.3 5.5 5.7 6.6 6.6 6.8 7.0 8.1 7.0
200 150 100 50 TT 16.2 0.2 ℄ 100.0 200 300 600

5.9 5.4 5.8 5.0 5.2 5.2 5.7 5.8 4.8
30.0 2.0 19.0 16.5 15.0 ℄ 2.0 2.5 30.0

7.0 7.5 6.8 6.9 7.2 7.0 7.7 7.0 6.5
30.0 19.0 16.5 14.0 ℄ 2.0 4.5 4.0 30.0

6.3 6.1 6.5 6.1 6.2 6.7 5.7 5.7
30.0 16.5 15.5 9.5 ℄ 5.0 4.0 30.0

4.4 4.6 5.7 5.6 5.3 3.7
30.0 21.5 14.0 ℄ 3.5 30.0

2.9 2.9 3.8 3.5 3.8 4.1 3.3 1.4
30.0 20.0 17.5 15.0 ℄ 2.5 4.5 30.0

8.3 7.8 8.1 7.7 7.2 7.3 8.2 7.2 6.9
30.0 16.5 15.5 13.5 ℄ 2.0 9.0 4.5 30.0

5.7 6.2 6.7 6.5 5.7 5.9 6.7 6.1 5.5
30.0 19.0 17.0 13.5 ℄ 3.0 5.0 2.5 30.0

5.3 5.3 5.2 4.3 3.7 4.0 5.0 3.9 3.5
30.0 19.0 13.5 9.5 ℄ 3.5 2.0 10.5 30.0

1.9 1.9 0.9 0.8 1.0 1.5 0.9 1.4
30.0 14.0 8.0 ℄ 4.0 6.0 8.5 30.0

11.1 10.1 11.6 11.3 11.7 9.9 10.9
30.0 7.5 5.0 ℄ 8.0 11.5 30.0

6.7 6.7 9.1 9.0 9.0 5.8 9.2
30.0 8.0 3.5 ℄ 8.0 16.5 30.0

		1277.93			
	15.13	1290.71	2.35	1275.58	
16.			14.2	1276.5	6.5/50.0 3.6/30.0 2.1/20.0 15.0/15.5 9.9/12.5 14.2/℄ 15.4/3.5 15.4/15.0 14.1/18.0 7.2/34.5 8.5/40.0 10.8/50.0
15+60			12.5	1278.2	6.7/50.0 3.8/30.0 3.1/17.0 8.4/11.0 12.5/℄ 14.3/4.5 14.2/16.5 11.6/22.5 7.6/29.5 8.7/33.0 10.5/50.0
15			15.0	1275.7	17.8/35.0 15.9/13.5 14.9/6.5 15.0/℄ 16.1/16.5 14.6/21.0 14.7/30.0
	2.86	1277.92	15.65	1275.06	
14			6.6	1271.3	11.1/30.0 7.9/5.0 6.9/2.5 6.6/℄ 5.9/5.0 6.0/14.0 6.3/15.0 5.9/15.5 3.6/30.0
13			7.8	1270.1	11.9/30.0 9.8/10.5 9.5/9.0 8.7/6.5 7.8/℄ 7.3/10.0 7.8/12.0 7.3/13.0 4.9/30.0
12			8.6	1269.3	10.3/30.0 9.4/10.0 8.9/7.5 8.6/℄ 8.5/9.0 8.7/10.0 8.4/11.0 5.8/30.0
11+34			8.9	1269.0	17.7/200. (1260.2) 13.2/100.0 (1264.7) 10.1/9.0 (1267.8) 9.5-9.4-9.2/5.8 (1268.4, 1268.5, 1268.7) 8.9/℄ (1269.0) 8.4-9.3-9.7/10.5 (1269.0, 1268.6, 1268.2) 5.3/75.0 (1272.6)
11			8.6	1269.3	11.0/30.0 9.5/9.5 8.7/5.5 8.6/℄ 8.6/10.0 8.9/11.0 8.7/12.5 8.6/30.0
10			5.2	1272.7	6.5/30.0 5.6/8.0 5.0/6.5 5.4/5.0 5.2/℄ 5.0/12.5 5.7/14.0 5.3/15.5 5.3/17.5 2.9/25.0 2.3/30.0
	4.84	1278.44	4.32	1273.60	
9			5.4	1273.0	8.5/30.0 6.9/11.0 7.2/9.0 6.1/7.0 5.4/℄ 5.0/11.5 5.8/16.0 5.6/19.0 4.1/30.0 2.7/50.0
B.M			3.17	1275.27	
8+40			4.2	1274.2	6.2/30.0 4.6/9.0 4.3/7.0 4.2/℄ 4.0/9.0 4.3/14.5 4.0/11.0 4.9/13.0 3.1/15.0
T.P.	14.60	1291.91	1.13	1277.31	Spike in Ground near Grape post

		1291.91		
8+40			17,7	1274,2
8			17,5	1274,4
	0,81	1278,12		1277,31
8			3,7	1274,4
	8,37	1282,43	4,06	1274,06
7+48			8,4	1273,8
7			7,7	1274,7
6			3,7	1278,7
5+40			2,20	1280,2
5			3,6	1278,6
	7,72	1285,93	4,22	1278,21
4+40			7,4	1278,5
4			7,4	1278,5
3			6,6	1279,3
2			4,8	1281,1
1			7,7	1278,2

17,7 / 2 — 5,2 / 40,0 — 3,2 / 50,0

17,5 / 2 — 6,8 / 4,0 — 4,3 / 50,0

6,5 / 30,5 — 4,4 / 10,0 — 3,9 / 8,5 — 3,7 / 2 — 4,2 / 8,0 — 4,4 / 10,0 — 4,0 / 13,0

12,6 5,4 — 12,6 8,5 — 1271,5 — 1272,4 — 1273,1 — 12 7,35 — 1273,8 — 1273,1 — 1272,0 — 1270,93 — 1275,3

17,0 / 200,0 — 13,9 / 100,0 — 19,5 — 10,0 — 23 / 8,0 — 8,6 / 2 — 8,6 / 12,0 — 9,3 10,4 11,5 / 16,0 — 7,1 / 30,0

6,6 / 30,0 — 7,6 / 7,0 — 8,0 / 6,0 — 7,6 / 3,0 — 7,7 / 2 — 7,7 / 13,0 — 7,3 / 14,5 — 7,6 / 16,5 — 5,9 / 30,0

3,8 / 30 — 3,0 / 7,0 — 4,0 / 7,0 — 3,7 / 2 — 3,9 / 12,0 — 3,1 / 17,0 — 5,2 / 19,6 — 1,6 / 23,0 — 1,6 / 30,0

5,0 / 30,0 — 3,8 / 9,5 — 4,2 / 8,0 — 3,6 / 2 — 3,5 / 13,0 — 3,7 / 17,5 — 1,4 / 26,0 — 1,3 / 30,0

1269,2 — 1273,6 — 1277,4 — 1277,6 — 1278,3 — 1278,5 — 1278,3 — 1278,0 — 1277,6 — 1281,6

16,7 / 200,0 — 12,9 / 100,0 — 8,5 — 8,3 — 7,6 / 5,8 — 7,4 / 2 — 7,4 — 7,8 — 7,3 / 10,6 — 4,3 / 100

8,6 / 30,0 — 7,8 / 9,0 — 8,3 / 8,0 — 7,6 / 5,5 — 7,4 / 2 — 7,5 / 8,5 — 8,1 / 10,5 — 7,4 / 12,0 — 7,9 / 30,0

7,4 / 30,0 — 6,8 / 10,0 — 7,2 / 7,0 — 6,6 / 2 — 6,5 / 9,0 — 7,0 / 10,5 — 5,8 / 13,0 — 5,2 / 30,0

6,6 / 30,0 — 5,1 / 9,5 — 6,0 / 8,0 — 4,8 / 2 — 5,3 / 9,5 — 3,8 / 12,5 — 2,6 / 30,0

8,5 / 30,0 — 7,8 / 10,5 — 8,6 / 9,0 — 8,2 / 6,5 — 7,7 / 2 — 8,1 / 9,0 — 7,3 / 11,0 — 6,0 / 30,0

		1285.93		
	3.44	1281.98	7.39	1278.54
0+00			4.8	1277.2
B.M			6.32	1275.66
-100			6.6	1275.4
-200			8.4	1273.6
-300			8.2	1273.8

$\frac{8.0}{30.0}$ $\frac{6.2}{10.0}$ $\frac{5.3}{7.0}$ $\frac{4.8}{\text{C}}$ $\frac{4.9}{7.5}$ $\frac{5.9}{12.0}$ $\frac{4.9}{17.0}$ $\frac{4.0}{30.0}$

S. E root 16" Maple 26 Lt Sta 0+10.

Dec. 31, 1929, Fair, 10" Snow on Ground.
W.C. Marks & David R. Parks went over road, estimating drainage Areas to determine sizes of pipe required.

Culvert

B. M.	3.42	1264.13	1260.71	
120+55		Elev. of footer Rt.		1254.0
		"	Lt.	1254.0

W. root 30" Elm, 25' Left, sta, 124+43

10.13	4.63	C 5'6" stake 30' Rt
10.13	6.13	C 4'0" stake 30' Lt

B.M	10.64	1286.30		1275.66	
0					1276.60
1					1278.80
2					1280.60
T.P.	7.11	1286.48	6.93	1279.37	
3					1279.70
4					1279.00
5					1279.00
6					1278.70
7					1276.00
	1.18	1277.57	10.09	1276.39	
8					1274.40
9					1273.40
10					1272.40
11					1269.50
12					1269.50
13					1270.50
T.P.			4.66	1272.91	
	11.74	1289.11	0.22	1277.35	
8					1274.40
T.P.	5.59	1278.50		1272.91	
14					1272.00
15					1275.50
T.P.	10.[illegible]	1286.[illegible]	2.07	1276.43	
16					

S.E. root 25'L sta. 0-10

9.70	11.10	F1.4 / 23.0	8.22	C1.5 / 26.0
7.50	7.95	F0.5 / 24.0	6.38	C1.1 / 25.0
5.70	6.09	F0.4 / 24.6	3.09	C2.6 / 28.0
6.78	7.31	F0.5 / 23.0	5.65	C1.1 / 26.0
7.48	8.78	F1.3 / 23.0	8.15	F0.7 / 24.0
7.48	8.16	F0.7 / 23.0	5.45	C2.0 / 26.5
7.78	7.41	C0.4 / 25.0	5.40	C2.4 / 28.0
16.48	10.08	C0.4 / 24.0	9.60	C0.9 / 24.0
3.17	5.30	F2.1 / 22.5		
4.17	6.90	F2.7 / 23.0	4.34	F0.2 / 23.5
5.17	5.45	F0.3 / 24.0	2.05	C8.1 / 29.0
8.07	9.75	F1.7 / 23.0	6.24	~~C1.8~~ F0.3 / 24.8
8.07	9.20	F1.1 / 23.0	5.53	C2.5 / 27.0
7.07	10.30	F3.2 / 24.5	4.46	C2.4 / 27.0

Slope hub rt sta. 13+00

14.71			5.45	C9.3 / 33.0

Slope hub Rt. sta. 13+00

6.50	10.75	F4.3 / 25.0	4.46	C2.0 / 26.5
3.08	4.11	F1.1 / 19.0	2.05	C1.0 / 25.5

Slope hub RT sta 16+00

T.P.	10.22	1286.65		1276.43	
15+60					1276.50
	6.64	1291.48	1.83	1284.82	
16					1275.50
	1.84	1281.06	12.24	1279.22	
15+60					1276.50
16					1275.50
	5.01	1275.19	10.88	1270.18	
17					1270.00
17+40					1267.80
	4.08	1268.50	9.77	1265.42	
17+40					1267.80
18					1264.50
19					1261.30
	3.25	1262.96	9.85	1259.65	
20					1259.40
21					1257.50
22					1255.60
	6.42	1261.53	7.79	1255.11	
22					1255.60
23					1254.40
24					1253.20
	4.16	1256.67	9.02	1252.51	
25					1252.40
26					1251.80

Slope hub Rt. Sta. 15700

10.15	1.83	C 8.3 / 33.0			
15.98	4.51	C 11.5 / 33.0			
4.56			2.92	C 1.6 / 18.0	
5.56			4.12	C 1.4 / 18.5	
5.19	4.02	C 1.2 / 27.0	5.01	C 0.2 / 25.5	
7.39			8.43	F 1.0 / 24.5	
1.70	3.09	F 1.4 / 24.0			
5.00	6.46	F 1.5 / 22.5	6.27	F 1.3 / 23.0	
8.20	10.05	F 1.9 / 22.0	8.39	F 0.2 / 24.0	
3.50	4.18	F 0.6 / 24.0	3.49	0.0 / 24.0	
5.40	5.23	C 0.2 / 24.0	4.34	C 1.1 / 26.0	
7.30			4.88	C 2.5 / 27.5	
5.93	4.88	C 1.1 / 26.0			
7.13	6.64	C 0.5 / 25.0	1255.44 / 6.09	C 1.0 / 25.5	
8.33	8.49	F 0.2 / 25.0	8.00	C 0.3 / 24.5	
4.27	4.17	C 0.1 / 24.0	3.12	C 1.2 / 25.0	
4.87	1251 A 8 / 5.19	F 0.3 / 24.5	4.65	C 0.2 / 24.5	

		1256.67			
27					1251.50
	3.01	1254.81	4.87	1251.80	
28					1250.60
29					1249.00
	2.38	1253.16	4.03	1250.78	
B.M			1.57	1251.57	
				1251.46	recoFd

5.17	3.51	C 1.7 / 27.0	4.76	C 0.4 / 25.0
4.21	2.30	C 1.9 / 27.0	4.98	F 0.8 / 23.5
5.81	4.02	C 1.8 / 27.5	7.41	F 1.6 / 21.0

N. W. root 24" Cherry 28'L, Sta 29+49

B. M.	1.24	1252.70		1251.46	
30					1248.00
31					1247.00
	7.39	1259.07	1.02	1251.68	
32					1252.50
33					1254.00
	5.04	1258.96	5.15	1253.92	
34					1254.70
35					1255.40
	7.65	1263.02	3.59	1255.37	
36					1256.70
37					1258.00
38					1259.30
B. M.			2.80	1260.22	
	2.80	1263.02		1260.22	record
	3.25	1264.09	2.18	1260.84	
39					1259.60
40					1259.00
T. P.	2.26	1261.40	4.95	1259.14	
41					1258.00
42					1257.00
43					1256.00
			5.99	1255.41	

N. W. root 24" Cherry 28' Lt, Sta 29+49

~~4.70~~ ~~3.16~~ 3.70 ~~2.16~~	6.75	~~F0.5~~ F2.1 / 21.5 ~~F3.1~~ F1.9 / 21.5	7.75	~~F1.2~~ F3,1 / 24.0 ~~F1.1~~ F1.2 / 22.5 0.0
5.60			3.67	
6.57	3.95	C2.6 / 27.5	4.74	C1.6 / 27.5
5,07	5,13	F0.1 / 24.0	4.47	C0.6 / 27.5
4,26	5,04	F0.8 / 24,0	3.63	C0,6 / 25,0
3,56	3,60	0.0 / 25.0	1.41	C2.2 / 25.5
6,32	6,86	F0.6 / 24.0	5.39	C0.9 / 25.5
5,02	5,28	F0.3 / 24.0	4,32	C0.7 / 24,5
3,72	3,88	F0.2 / 24.5	2,57	C1.2 / 24.5

W, root 24" Maple, 24' R. Sta 37+41

4,49	4.69	F0.2 / 24.0	3,35	C1.1 / 25.0
5.09	4,96	C0.1 / 25.5	3.71	C1.4 / 25.0

2 Nails in stump 15' RT Sta 40+70

3.40	2,99	C0.4 / 25,0	1.78	C1.6 / 26.0
4,40	4,06	C0.3 / 26,0	3,96	C0.4 / 25.5
5,40	6.32	F0.9 / 23.5	5,99	F0.6 / 23,0

Slope hub RT. Sta. 43+00

July 25 1930
D. Parks
T. Snyder
R. Hassell

T.P.	5.03	1260.44		1255.41	
44					1256.00
45					1256.00
T.P.	3.94	1260.49	3.89	1256.55	
46					1256.00
47					1256.00
B.M					
48					1255.30
T.P.	3.86	1260.02	4.33	1256.16	
B.M			2.29	1257.73	
B.M.	2.29	1259.96		1257.67	Reg. 1257.67
T.P.	4.88	1259.44	5.40	1254.56	
49					1254.60
50					1253.90
T.P.			5.21	1254.23	

Hub. Right, Sta. 43+00

44	5.40 (1255.04)	FL.0 / 24.0	3.74	C0.7 / 25.0
4.44	5.59	F1.7 / 23.0	3.09	C1.4 / 26.5
4.49	5.03	F0.5 / 24.0	3.19	C1.3 / 25.5
4.49	5.28	F0.8 / 22.0		C1.3 / 27.5
5.19	5.87	F0.7 / 24.0	4.93	C0.3 / 26.0

W. Root 20" Maple, R. Sta. 47+20

4.84	4.88	0.0 / 25.5	4.38	C0.5 / 25.0
5.54	5.21	C0.3 / 25.5	4.23	C1.3 / 24.5

Slope hub. Left, Sta. 50+00

T.P.	2.46	1256.69		1254.23	
51					1253.20
52					1253.50
53					1254.50
	6.24	1261.45	1.30	1255.39	
54					1255.50
55					1256.50
56					1257.50
57					1258.00
58					1257.50
	8.19	1268.20	1.64	1260.01	
59					1261.30
B.M			1.03	1267.17	
	1.03	1268.20		1267.17	record
60					1263.10
60+30					1263.60
61					1264.00
62					1264.00
	4.93	1271.78	1.35	1266.85	
63					1264.50
64					1266.00
65					1267.00
66					1267.50
67					1267.00
68					1265.50

July 26. 1930 — D. Parks, T. Snyder, R. Hassell — 47

Sun Hot

Slope hub, Left Sta 50+00

3.39	4.34	F1.0 / 24.0	4.66	F1.3 / 23.0
3.19	4.18	F1.0 / 24.0	3.23	0.0 / 25.0
2.19	2.60	F0.5 / 24.5	1.55	C0.6 / 25.5
6.15	6.38	F0.2 / 25.0	5.10	C1.1 / 25.5
5.15	5.08	C0.1 / 25.0	3.93	C1.2 / 26.0
4.15	4.00	C0.2 / 24.5	5.54	F1.4 / 23.0
3.15	4.42	F1.5 / 23.0	1.90	C1.3 / 26.0
2.15	3.95	F1.8 / 21.0	1.38	C0.8 / 25.5
6.90	8.19	F1.3 / 23.5	3.61	C3.3 / 28.5

W. root 24" Maple

5.10	4.05	C1.1 / 24.5	2.01	C3.1 / 31.0
4.60	3.44	C1.2 / 26.5	1.26	C3.3 / 31.0
4.20	5.72	F1.7 / 23.0	3.84	C0.7 / 24.5
4.20	6.02	F1.9 / 23.0	5.12	F0.9 / 24.0
7.28	9.10	F1.8 / 23.0	8.10	F0.8 / 24.0
5.78	5.00	C0.8 / 26.5	4.12	C1.7 / 27.5
4.78	4.41	C0.4 / 25.5	3.92	C0.9 / 26.0
4.28	5.74	F1.5 / 23.0	4.05	C0.2 / 25.0
4.78	5.35	F0.6 / 24.5	3.58	C1.2 / 27.0
6.28	7.08	F0.8 / 24.5	5.74	C0.5 / 25.5

		1271.78			
	6.17	1271.69	7.06	1264.72	
69					1265.00
70					1265.00
70+60					1265.00
71					1265.00
72					1263.00
	5.93	1266.87	11.25	1260.44	
73					1262.00
B.M.			2.48	1263.89	
				1264.03	record
74					1262.00
75					1261.00

Void

B.M.	2.48	1266.51		1264.03	
73					1262.50
72					1263.00
	9.29	1269.96	5.84	1260.67	
71					1266.00
70+60					1265.00
70					1265.00
69					1265.00
	7.38	1270.64	6.70	1263.26	
68					1265.50
67					1267.00

6.69	8.52	F1.8 / 22.0		6.97	F0.3 / 25.0
6.69	7.80	F1.1 / 23.5		4.63	C2.1 / 28.0
6.69	6.68	0.0 / 23.5		3.58	C3.1 / 31.5
6.69	6.25	F0.3 / 24.5		4.04	C2.7 / 29.0
8.69	11.15	F2.5 / 22.0		9.15	F0.5 / 24.0
3.87	5.93	F2.1 / 21.0		2.46	C1.4 / 26.5

Void

S. W. root 24" Maple, 32' R., Sta. 73+95

S. W. root 24" Maple, 32' R., Sta. 73+95					
4.61	5.96	F2.0 / 21.0		2.48	C1.5 / 26.5
3.51	5.84	F2.3 / 22.5		3.84	F0.3 / 24.0
4.96	5.07	F0.1 / 24.5		2.28	C2.8 / 28.0
4.96	4.82	C0.1 / 25.5		1.72	C3.2 / 31.5
4.96	5.93	F1.0 / 23.5		2.72	C2.2 / 28.0
4.96	6.70	F1.7 / 22.0		5.10	F0.1 / 25.0
5.14	5.80	F0.7 / 24.5		4.46	C0.7 / 25.5
3.64	4.07	F0.4 / 24.5		2.28	C1.4 / 27.0

		1270,64			
66					1267,50
	4,70	1272,61	2,73	1267,91	
65					1267,00
64					1266,00
63					1264,50
	5,16	1268,18	9,66	1262,95	
62					1264,00
61					1264,00
60+30					1263,60
60					1263,00
B.M.			0,85	1267,26	
				1267,17	record

		F1,3		C0,4
3,14	4,45	23,0	2,73	25,0
		C 0,6		C0,1
5,61	4,97	25,5	4,52	26,0
6,61	5,56	C1,1	4,68	C1,9
		26,5		27,5
8,11	9,66	F1,6	8,67	F0,6
		23,0		27,0
	1262,21	F1,8		F0,8
4,11	5,90	23,0	4,93	24,0
4,11	5,74	F1,6	3,72	C0,4
		23,0		27,6
4,61	3,22	C1,3	1,12	C3,4
		24,5		31,0
5,01	3,88	C1,1		C3,2
		26,5		31,0

W. root 24" Maple

B.M.	2.35	1266.38		1264.03	
74					1262.00
75					1261.00
76					1259.10
	2.80	1260.66	8.52	1257.86	
77					1257.80
78					1256.50
79					1255.80
80					1255.70
	4.90	1260.51	5.05	1255.61	
81					1255.70
82					1255.70
83					1255.70
84					1255.20
85					1254.61
	4.42	1257.39	7.54	1252.97	
86					1253.60
87					1252.60
88					1252.60
B.M			6.19	1251.20	
				1251.23	record

July 27, 1930
cloudy, showers

D. Parks
T. Snyder
R. Hassell

S. W. root 24" Maple, 32' R, Sta. 73+95

4.38	6.21	F1.8 / 20.0	3.00	C1.4 / 27.0
5.38	6.75	F1.4 / 23.0	3.32	C2.1 / 27.5
7.28	7.78	F0.5 / 24.5	6.16	C1.1 / 28.0
2.86	4.30	F1.4 / 23.0	2.80	C0.1 / 25.0
4.16	4.78	F0.6 / 24.5	4.30	F0.1 / 24.0
4.86	5.73	F0.9 / 24.0	3.88	C1.0 / 25.0
4.96	5.46	F0.5 / 25.0	5.46	F0.5 / 23.5
4.81	5.35	F0.5 / 24.5	4.90	F0.1 / 24.0
4.81	4.40	C0.4 / 25.0	4.12	C0.7 / 25.0
4.81	4.70	C0.1 / 25.0	3.72	C1.1 / 25.5
5.31	5.00	C0.3 / 25.5	4.60	C0.7 / 23.0
5.91	5.21	C0.7 / 25.5	5.84	C0.1 / 23.0
3.79	3.50	C0.3 / 25.0	3.75	0.0 / 23.0
4.79	5.90	F1.1 / 23.5	5.16	F0.4 / 23.0
4.79	6.10	F1.3 / 23.5	6.08	F1.3 / 22.5

E. root, 18" Hickory 33' L, Sta. 88+04

120+55	0.55	1259.80		1259.25
				1256.0
300± West			5.1	1254.7
450±			5.9	
500± W. to Fence			6.1	1253.7
650± 150 S.W. from ditch at Fence			7.5	1252.3
850±			9.0	1250.8

July 29, 1930 Marks, Belding. Fair, 75° 46

Top of Opening of Culvert.
Flow Line at Culvert.

3.9	5.1	3.6
20' South	ditch	20' North.
5.2	5.9	5.0
	ditch	
5.0		4.9

Pipe Culverts

B.M.	9.38	1285.04		1275.66	
4+40					
T.P.	3.25	1279.66	8.63	1276.41	
7+48					
T.P.	1.64	1276.96	4.36	1275.30	
11+34					
23+57,	15" Corr. Pipe Side Road Culvert, 40' Long				
	4.10	1259.54		1255.44	
			5.68		1251.36
			4.96		1252.08
26+30±	24" Corr. Pipe Culvert, 42' Long,				
	5.13	1256.71		1251.48	
			4.66		1249.05
			5.26		1248.45

Aug. 7, 1930 D. Parks
R. Hassel
Fair 80° E. Belding
S.E. root 25' L, Sta. 0-10

1277.00	8.04	6.04 C2'0" Stake 30' Right
1276.39	8.65	7.15 C1'6" Stake 30' Left
1271.04	8.62	6.12 C2'6" Stake 30' Right
1270.43	9.23	7.73 C1'6" Stake 30' Left

R.P. Spike S. side

1267.31	9.65	6.65	C3'0" Stake 30' Right
1266.70	10.26	8.76	C1'6" Stake 30' Left

Aug. 12, 1930 Fair, 65°, Marks, Snyder, Wilder.
Slope Hub, 25.5' R., 23+00

8.18	C 2'6"	Stake 19' R, 23+87
7.46	C 2'6"	Stake 19' R, 23+27

Slope Hub, 24.5' L. 26+00

7.66	Cut 3'	Stake, 30' L.
8.26	Cut 3'	Stake, 30' R.

B. M.	8.42	1259.65		1251.23	
89					1252.60
90					1253.80
91					1255.30
92					1256.80
	6.69	1265.71	0.63	1259.02	
93					1258.30
94					1259.80
95					1260.70
96					1261.60
97					1262.50
98					1263.00
	8.06	1272.39	1.38	1264.33	
99					1264.60
100					1266.50
B. M.			1.53	1270.86	
				1270.81	record

Aug. 7 1930 D. Parks R. Hassel E. Belding

75° Clear Warm Wind

E. root 18" Hickory 33' L., Sta. 88+06

7.05	7.10	F0.1 / 25.0	6.02	C1.0 / 25.5
5.85	5.84	0.0 / 23.0	5.29	C0.6 / 25.5
4.35	4.78	F0.4 / 24.0	4.41	F0.1 / 24.5
2.85	2.93	F0.1 / 25.0	2.67	C0.2 / 25.0
7.41	7.06	C0.4 / 25.5	3.59	C3.8 / 28.0
5.91	6.67	F0.8 / 24.0	4.55	C1.4 / 24.5
5.01	6.20	F1.2 / 24.0	2.81	C2.2 / 27.5
4.11	4.79	F0.7 / 24.0	1.15	C3.0 / 28.0
3.21	3.87	F0.7 / 24.0	2.09	C1.1 / 25.0
2.71	4.49	F1.8 / 23.0	3.14	F0.4 / 24.0
7.79	8.06	F0.3 / 25.0	7.74	C0.1 / 24.5
5.89	6.45	F0.6 / 24.0	3.40	C2.5 / 28.0

R. P. Spike N. W. root 30" Maple

44+50 15" Corr. Pipe Culvert, 40' Long.

5.13	1260.17	1255.04	
		2.52	1254.13
		4.42	1253.25
5.25	1269.28	1264.03	
71 Check on Slope Hubs,			1265.00

61+76 18" Corr. Pipe Culvert. 40' Long

6.40	1268.61	1262.21	
		5.71	1261.50
			1260.90

Slope Hub, 44+00 Left.

8.02	Cut 3'6"	Stake 30' R.
6.92	Cut 2'6"	Stake 30' L.

B.M. S.W. Root 24" Maple, 32' R. 73+95

4.28	4.42	F1.4	1.50 C 2.8

Slope Hub, 62+00 Left

7.11	Cut 3'	Stake 30' R.
7.71	Cut 2'	Stake 30' L.

B. M.	2,40	1273.21		1270.81	
101					1266.70
102					1266.90
103					1267.10
104					1267.30
105					1266.60
	5,66	1271,19	7.68	1265,53	
106					1265.20
107					1263.80
108					1262.40
109					1261.00
	6.19	1267.22	10.14	1241.03	
110					1259.60
111					1259.00
112					1259.40
	7.80	1266.60	8.42	1258.80	
113					1259.80
114					1260.60
B. M.			2.00	1264.60	
				1264.67	record

Aug. 15. 1930 — D. Parks, R. Hassel, T. Snyder
85° Windy

5

R.P. Spike N.W. root 30" Maple

			F1.7				C1.0
6,51		8,21	21.0		5,54		26.5
			F2.8				C0.1
6,31		9,14	23.0		6,18		24.5
			F0.7				C1.5
6.17		6,85	24.0		4,57		26.0
			F0.6				C2.2
5,91		6.53	24.5		3.75		28.0
			F0.9				C0.7
1266,45	6.76	7.68	24.0	1267.05	6.16	5.44	25.5
			C0.5				C1.7
1265.05	6.14	5.61	26.5	1265.65	5.54	3,89	26.0
			C0.1				C0.3
1263.65	7.54		25.0	1264.25	6.94	6.63	25.5
			F1.7				F0.2
8,79		10.47	23.0		8,98		24.0
			0.0				C1.0
10,19		10.16	26.0		9.22		26.0
			F0.2				C2.1
7,62		7.83	26.0		5,49		27.5
			F1.0				F0.4
8,22		9,22	23.5		8,58		23.5
			F1.0				F0.4
7,82		8,86	23.5		8.42		23.5
			C0.4				C2.4
4,88		6,35	25.0		4,18		28.0
			F1.0				C2.3
6.08		6,96	23.5		3,73		27.5

S.W. side 30" Maple - (R.P. Spike)

B.M.	0.89	1265.56		1264.67	
115					1261.10
116					1261.60
~~117~~	5.62	1267.11	4.07	1261.49	~~1262.10~~
117					1262.10
117+54					1262.10
118					1261.70
	3.76	1263.71	7.16	1259.95	
119					1260.00
120					1260.00
121					1260.00
122					1260.00
123					1260.00
124					1260.00
B.M.			2.97	1260.74	
	4.66	1265.37		1260.71	record
125					1260.00
126					1260.70
127					1261.40
128					1262.10
	5.00	1267.49	2.88	1262.49	
129					1262.80
130					1263.50

Aug. 16. 1930 — D. Parks, T. Snyder, R. Hassel

Showers

S. W. side 20" Maple (R.P. spike)

4.46	4.43	0.0 / 25.5	3.43	C1.0 / 26.5
3.96	4.83	F0.9 / 27.0	2.41	C1.6 / 27.0
~~3.46~~				
5.01	5.15	F0.1 / 24.5	3.98	C1.0 / 26.0
5.01	3.84	C1.2 / 26.5	2.41	C2.6 / 28.5
5.41	4.37	C1.0 / 26.5	3.49	C1.9 / 27.5
3.71	3.76	F0.1 / 25.0	2.61	C1.1 / 26.0
3.71	4.75	F1.0 / 23.0	3.98	C0.3 / 23.0
3.71	5.76	F2.1 / 33.0	3.60	C0.1 / 33.0
3.71	5.30	F1.6 / 33.0	5.33	F1.6 / 33.0
3.71	5.17	F1.5 / 33.0	4.76	F1.1 / 33.0
3.71	4.33	F0.6 / 30.0	4.04	F0.4 / 33.0

W. root 30" Elm L Sta. 124+43

5.37	5.33	0.0 / 28.0	5.02	C0.4 / 33.0
4.67	4.85	F0.2 / 28.5	3.99	C0.7 / 33.0
3.97	3.82	C0.2 / 25.5	2.98	C1.0 / 33.0
3.27	2.90	C0.4 / 25.5	1.57	C1.7 / 33.0
4.69	5.00	F0.3 / 24.5	5.00	F0.3 / 33.0
3.99	4.24	F0.3 / 25.0	6.01	F2.0 / 30.0

Aug 19, 1930
Cloudy

D. Parks
G. Wilder

S. E root 25' Lt Sta 0-10

					Grade Elev.
B.M.	6.37	1282.03		1275.66	
0+00			5.1	1276.9	1276.60
1+00			3.8	1278.7	1278.80
2+00			1.5	1280.5	1280.60
3			2.3	1279.7	1279.70
4			2.8	1279.2	1279.00
5			2.6	1279.4	1279.00
6			3.4	1278.6	1278.70
7			5.8	1276.2	1276.00
T.P.	2.14	1278.55	5.62	1276.41	
8			3.9	1274.7	1274.40
9			5.2	1273.4	1273.40
10			6.4	1272.2	1272.40
11			8.8	1269.8	1269.60
12			8.9	1269.7	1269.60
13			8.1	1270.5	1270.60
14			6.5	1272.1	1272.00
15			3.1	1275.5	1275.60
16			2.8	1275.8	1275.60
T.P.	0.39	1277.28	1.44	1276.89	
17			7.3	1270.00	1270.00
18			12.7	1264.6	1264.60
T.P.	1.32	1267.97	10.63	1266.65	
19			6.6	1261.4	1261.30
20			8.5	1259.5	1259.40

		1267.97			
21			10.4	1257.6	1257.50
22			12.2	1255.8	1255.60
T.P.	1.19	1256.59	12.57	1255.40	
23			2.2	1254.4	1254.40
24			3.5	1253.1	1253.20
25			4.3	1252.3	1252.40
26			4.7	1251.9	1251.80
27			5.1	1251.5	1251.50
28			6.0	1250.6	1250.60
29			7.7	1248.9	1249.00
T.P.	5.44	1252.85	9.18	1247.41	
B.M.			1.35	1251.50	N.W. root 24" cherry, 28' L. sta. 29+49
	3.28	1254.74		1251.46	record
30			6.6	1248.1	1248.00
31			5.2	1249.5	1249.00
32			2.2	1252.5	1252.50
33			0.8	1253.9	1254.00
T.P.	8.92	1263.07	0.59	1254.15	
34			8.4	1254.7	1254.70
35			7.6	1255.5	1255.40
36			6.4	1256.7	1256.70
37			5.3	1257.8	1258.00
38			4.0	1259.1	1259.30
B.M.			2.91	1260.16	W. root 24" Maple 24' Rt. sta 37+41

B.M.	2.91	1263.13		1260.22	
39			3.7	1259.4	1259.60
40			4.2	1258.9	1259.00
41			4.9	1258.2	1258.00
42			6.0	1257.1	1257.00
43			6.9	1256.2	1256.00
44			7.0	1256.1	1256.01
45			7.3	1255.8	1256.00
	5.35	1260.14	8.34	1254.79	
46			4.3	1255.8	1256.00
47			4.3	1255.8	1256.00
B.M			2.49	1257.65	
	2.49	1260.16		1257.67	record
48			5.0	1255.2	1255.30
49			5.3	1254.9	1254.60
50			6.2	1254.0	1253.90
51			6.6	1253.6	1253.20
52			6.3	1253.9	1253.60
53			5.8	1254.4	1254.50
54			4.6	1255.6	1255.50
	7.81	1261.98	5.99	1254.17	
55			5.4	1256.6	1256.50
56			4.5	1257.5	1257.50
57			3.6	1258.4	1258.50
58			2.4	1259.6	1259.50

W. root 24" Maple 24' Rt. sta. 37+41

W. root 24" Maple 40' Rt sta 47+20

		1261.98			
T.P.	8.40	1248.72	1.66	1260.32	
59			7.5	1261.2	1261.3
B.M.			1.51	1267.21	
				1267.17	record

W. root 24" Maple

Aug 20 1930 D. Parks
Cloudy 80° R. Hassel
W. root 24" Maple

B.M	3.39	1270.56		1267.17	
60			7.4	1263.2	1263.10
60+30			7.0	1263.6	1263.60
61			6.5	1264.1	1264.00
62			6.6	1264.0	1264.00
63			6.1	1264.5	1264.50
T.P	3.77	1271.63	2.70	1267.86	
64			5.6	1266.0	1266.00
65			4.4	1267.2	1267.00
66			4.2	1267.4	1267.50
67			4.6	1267.0	1267.00
68			6.0	1265.6	1265.50
69			6.7	1264.9	1265.00
70			6.5	1265.1	1265.00
T.P.			7.59	1264.04	

Slope hub Lt. Sta 70

B.M.	9.09	1284.75		1275.66			
0					1276.60	1277.20	7.55
1					1278.80	1279.40	5.35
2					1280.60	1281.20	3.55
3					1279.70	1280.30	4.45
4					1279.00	1279.60	5.15
5					1279.00	1279.60	5.15
	3.70	1282.75	5.70	1279.05			
5+40					1279.20	1279.80	2.95
6					1278.70	1279.30	3.45
7					1276.00	1276.60	6.15
8					1274.40	1275.00	7.75
	1.80	1276.80	7.75	1275.00			
8+40					1274.00	1274.60	2.20
9					1273.40	1274.00	2.80
10					1272.40	1273.00	3.80
11					1269.50	1270.10	6.70
12					1269.50	1270.10	6.70
	9.03	1279.12	6.71	1270.09			
13					1270.50	1271.10	8.02
14					1272.00	1272.60	6.52
15					1275.60	1276.10	3.02
T.P.			3.02	1276.10			

Finish Grade Stake Lt. Sta. 15

Aug. 25, 1930

Showers

D. Parks
R. L. Hassel
T. Snyder

S. E. root 25' Lt Sta 0-10

T.P	3.63	1279.73		1276.10		Finish	Grade	Stake Lt. sta 15
15+60					1276.50	1277.10	2.63	
16					1275.50	1276.10	3.63	
17					1270.00	1270.60	9.13	
17+40					1267.80	1268.40	11.33	
	1.11	1268.16	12.68	1267.05				
18					1264.50	1265.10	3.06	
19					1261.30	1261.90	6.26	
20					1259.40	1260.00	8.16	
	1.73	1261.73	8.16	1260.00				
21					1257.50	1258.10	3.63	
22					1255.60	1256.20	5.53	
23					1254.40	1255.00	6.73	
	2.72	1257.72	6.73	1255.00				
23+57	15" Corr. pipe	Side Rd. Culvert		+40' long				
					1251.36	6.36	4.86	C1'6" Stake 19' Rt, 23+87
					1252.08	5.64	3.14	C2'6" Stake 19' Rt, 23+27
24					1253.20	1253.80	3.92	
25					1252.40	1253.00	4.72	
26					1251.80	1252.40	5.32	
	2.00	1254.40	5.32	1252.40				
27					1251.50	1252.10	2.30	
28					1250.60	1251.20	3.20	
29					1249.00	1249.60	4.80	

	1254.40				
30				1248.00	1248,60 5.80
B.M.		2.97	1251,43		N W, root 24" cherry, 28' L Sta. 29+49
			1251.46	record	

Sept. 3. 1930
West Wind
Warm 80

D. Parks
R.L. Hassel

B.M	5.37	1256.83		1251.46			
31					1249.00	1249.60	7.23
32					1252.50	1253.10	3.73
33					1254.00	1254.60	2.23
34					1254.70	1255.30	1.53
	5.64	1260.95	1.52	1255.31			
35					1255.40	1256.00	4.95
36					1256.70	1257.30	3.65
37					1258.00	1258.60	2.35
38					1259.30	1259.90	1.05
B.M			0.76	1260.19			
	4.17	1264.39		1260.22	record		
39					1259.60	1260.20	4.19
40					1259.00	1259.60	4.79
T.P.			4.80	1259.59			

N.W. root 24" cherry, 28'Lt., sta. 29+49

W. root 24" Maple 24'Rt. sta. 37+41

finish Grade Stake Lt. Sta. 40+00

Sept. 8, 1930
Clear Warm

D. Parks
E. Parks
T. Snyder

B.M.	3.33	1267.36		1264.03		S. W. root 24" Maple, 32' Rt., Sta. 73+95			
73+64					1259.50	7.86	5.86	C 2'0"	stake 30' Lt
					1260.11	7.25	3.25	C 4'0"	stake 30' Rt
	5.44	1270.73	2.07	1265.29					
68+77					1262.10	8.63	7.13	C 1'6"	stake 30' Lt
					1262.71	8.02	4.52	C 3'6"	stak 30' Rt

T. P.	3.35	1262.94		1259.59	
41					1258.00
42					1257.00
	3.30	1259.67	6.57	1256.37	
43					1256.00
44					1256.00
45					1256.00
46					1256.00
	2.41	1259.88	2.20	1257.47	
47					1256.00
B.M.			2.16	1257.72	
	2.16	1259.83		1257.67	record
48					1255.30
49					1254.60
50					1253.90
	4.90	1258.52	6.21	1253.62	
51					1253.20
T. P.			3.45	1255.07	

Sept. 9, 1930 — D. Parks, T. Snyder, E. Parks — 62

Clear Warm 80°

Finish	Grade	Stake Lt. Sta. 40+00
1258.60	4.34	
1257.60	5.34	
1256.60	3.07	
1256.60	3.07	
1256.60	3.07	
1256.60	3.07	
1256.60	3.28	

W. root 24" Maple, 40' R., Sta. 47+20

1255.90	3.93
1255.20	4.63
1254.50	5.33
1253.80	4.72

X N.W. cor. E. Headwall

Sept. 9, 1930

D. Parks
T. Snyder
E. Parks

B. M.	0.28	1271.09		1270.81	B. M. Spike, N. W. root 30" Maple
97+94				1260.10	10.99 8.99 C 2' 0" Stake 30' Lt.
				1260.71	10.38 6.88 C 3' 6" Stake 30' Rt.

Sept. 10, 1930 D. Parks E. Parks

Clear Warm 80°

T. P.	3.94	1259.01		1255.07		
52					1253.50	X N.W. cor. E. Headwall
53					1254.50	1254.10 4.91
54					1255.50	1255.10 3.91
55					1256.50	1256.10 2.91
	6.69	1263.77	1.93	1257.08		1257.10 1.91
56					1257.50	1258.10 5.67
57					1258.50	1259.10 4.67
58					1259.50	1260.10 3.67
59					1261.30	1261.90 1.87
	6.23	1268.93	1.07	1262.70		
B.M.			1.67	1267.26		W. root 24" Maple
	1.67	1268.84		1267.17	record	
60					1263.10	1263.70 5.14
60+30					1263.60	1264.20 4.64
	6.62	1270.82	4.64	1264.20		finish Grade stake Lt sta. 60+30
61					1264.00	1264.60 6.22
62					1264.00	1264.60 6.22
63					1264.50	1265.10 5.72
64					1266.00	1266.60 4.22
65					1267.00	1267.60 3.22
66					1267.50	1268.10 2.72
	2.31	1270.49	2.64	1268.18		
67					1267.00	1267.60 2.89
68					1265.50	1266.10 4.39

		1270.49					
69					1265.00	1265.60	4.89
70					1266.00	1265.60	4.89
70+60					1265.00	1265.60	4.89
71					1265.00	1265.60	4.89
	2.16	1267.76	4.89	1265.60			
72					1263.00	1263.60	4.16
73					1262.50	1263.10	4.66
74					1262.00	1262.60	5.16
B.M			3.74	1264.02		S.W. root 24" Maple, 32' Rt., Sta 73+95	
				1264.03	record		

Sept, 13, 1950

Cloudy 75°

D. Parks
T. Snyder
R. Hassel
E. Parks

102+20	Sct & Graded.					
B.M	1.16	1265.83		1264.67		
	4.05	1264.19	5.69	1260.14		
110+99					1255.86	8.33 5.33 C3' Stake 30' Lt.
					1256.76	7.43 4.43 C3'0" Stake 30' Rt.
	1.59	1266.26		1264.67		
114+54					1257.80	8.46 5.46 C3' Stake 30' Lt.
					1258.70	7.56 4.56 C3' Stake 30' Rt.

Cut 4' Stake 30' Rt.
C 1' Stake 30' Lt.

S.W. side 20" Maple

B.M.	0.95	1264.98		1264.03	
75					1261.00
76					1259.10
77					1257.80
78					1256.50
	2.75	1259.84	7.89	1257.09	
79					1255.80
80					1255.70
81					1255.70
82					1255.70
83					1255.70
	1.86	1258.15	3.55	1256.29	
84					1255.20
85					1254.60
86					1253.60
87					1252.60
88					1252.60
B.M			6.94	1251.21	
	6.68	1257.91		1251.23	record
89					1252.60
90					1253.80
T.P.			3.51	1254.40	

Sept. 13, 1930

Cloudy 75°

D. Parks
T. Snyder
R. Hassel
E. Parks

S.W. root 24" Maple, 32' Rt. Sta. 73+95

1261.60	3.38
1259.70	5.28
1258.40	6.58
1257.10	7.88
1256.40	3.44
1256.30	3.54
1256.30	3.54
1256.30	3.54
1256.30	3.54
1255.80	2.35
1255.20	2.95
1254.20	3.95
1253.20	4.95
1253.20	4.95

E. root, 18" Hickory 33' L., Sta. 88+06

1253.20	4.71
1254.40	3.51

Finish Grade Stake Lt. Sta. 90+00

T. P.	7.87	1262,27		1254.40	
91					1255,30
92					1256.80
93					1258.30
94					1259.80
95					1260.70
	7.10	1268,40	0.97	1261,30	
96					1261.60
97					1262,50
98					1263.00
99					1264.60
100					1266.50
	4.89	1271,99	1.30	1267,10	
B. M.			1,17	1270,82	
				1270.81	Record

Sept. 20, 1930

Clear 75°

D. Parks
T. Snyder
R. Hassel

Finish Grade Stake Lt. Sta. 90+00

1255.90	6.37
1257.40	4.87
1258.90	3.37
1260.40	1.87
1261.30	0.97
1262.20	6.20
1263.10	5.30
1263.60	4.80
1265.20	3.20
1267.10	1.30

Spike, N.W. root, 30" Maple

B.M.	1.80	1272.41		1270.81	
101					1266.70
102					1266.90
103					1267.10
104					1267.30
105					1266.60
106					1265.20
107					1263.80
	0.82	1265.22	8.21	1264.40	
108					1262.40
109					1261.00
110					1259.60
111					1259.00
112					1259.40
113					1259.80
1. B.M.			0.52	1264.70	[illegible]
	1.07	1265.74		1264.67	record
114					1260.60

Sept. 22. 1930
Clear 75°

D. Parks
T. Snyder
R. Hassel

88

Spike, N.W. root 30" Maple

1267.30	5.31				
1267.50	5.11				
1267.70	4.91				
1267.90	4.71				
1267.20	5.41				
1265.80	1265.65	6.96	1266.25	6.36	
1264.40	8.21				
1263.00	2.22				
1261.60	3.62				
1260.20	5.02				
1259.60	5.62				
1260.00	5.22				
1260.40	4.82				

R.R. spike S.W. side 20" Maple

1261.20	4.54	

B.M.	2.29	1266.96		1264.67	
115					1261.10
116					1261.60
117					1262.10
117+54					1262.10
118					1261.70
119					1260.00
120					1260.00
	3.30	1264.61	5.65	1261.31	
121					1260.00
122					1260.00
123					1260.00
124					1260.00
B.M.			3.88	1260.73	
	3.88	1264.59		1260.71	record
125					1260.00
126					1260.70
	6.06	1267.38	3.27	1261.32	
127					1261.40
128					1262.10
129					1262.80
130					1263.50

Oct. 2, 1930
Clear Warm 75°

D. Parks
R. Hassel

S.W. side 20" Maple

1261.70	5.26
1262.20	4.76
1262.70	4.26
1262.70	4.26
1262.30	4.66
1260.60	6.36
1260.60	6.36
1260.60	4.01
1260.60	4.01
1260.60	4.01
1260.60	4.01

W. root 30" Elm L sta. 124+43

1260.60	3.99
1261.30	3.29
1262.00	5.38
1262.70	4.68
1263.40	3.98
1264.50	2.88

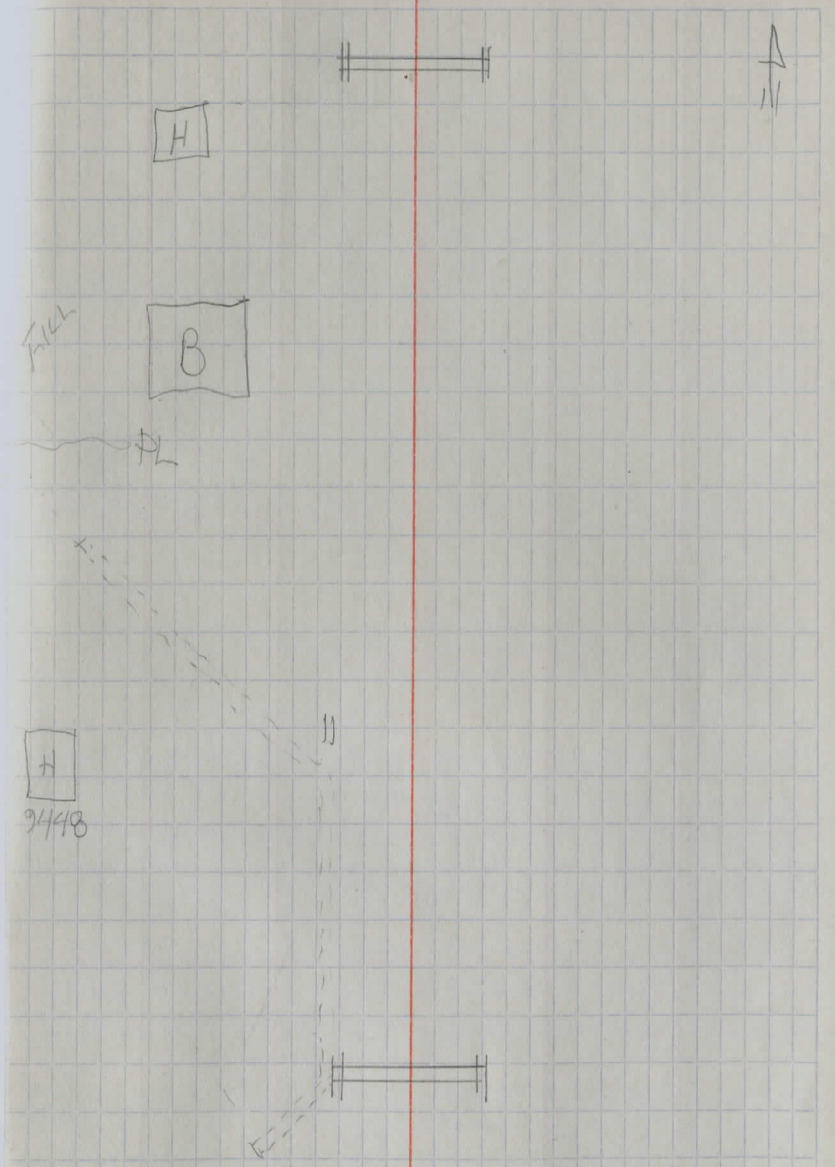
J. E. HERSHBERGER
D. W. SEWELL

DRAINAGE COMPLAINT
9448 CLAY CH 37 G

11 JUNE 1981
±70°F, FAIR, BREEZY

72

STA.	B.S.	H.I.	F.S.	ELEV.	
T.B.M. TOP MVD	5.50	105.50		100.00	SW COR. W HDWL. N CULV.
OUT N CULV. INV. OUT			8.67	96.83	W END
N CULV. TOP MVD			8.82	96.68	W END
IN N CULV. INV.			8.38	97.12	E END
IN N CULV. INV.			8.59	96.91	E END
OUT YARD DRAIN INV.			8.65	96.85	
IN DR. PIPE INV.			7.99	97.51	9448 CLAY
IN S CULV. INV. IN YD. DRAIN			7.72	97.78	E END
FL NAT. ELEV.			6.55	98.95	S END
N FL FILL			9.55	95.95	FLOW LINE FORMER FLOW LINE
			8.85	96.65	D.S. 6-11-81



KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle of Intersection or I. P.=23° 20′ to the R. at Station 542+72.

Ext. in Tab. IV opposite 23° 20′=120.87
120.87÷12=10.07. Say a 10° Curve.

Tan. in Tab. IV opp. 23° 20′=1183.1
1183.1÷10=118.31.

Tab. V. correction for A. 23° 20′ for a 10° Cur.=0.16
118.31+0.16=118.47=corrected Tangent.

(If corrected Ext. is required find in same way)
Ang. 23° 20′=23.33°÷10=2.3333=L. C.

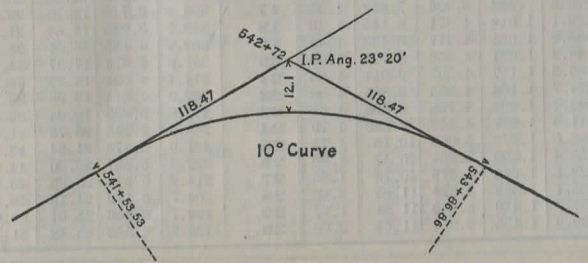
2° 19½′=def. for sta.	542	I. P.=sta.	542+72
4° 49½′= " " "	+50	Tan.=	1.18.47
7° 19½′= " " "	543	B. C.=sta.	541+53.53
9° 49½′= " " "	+50	L. C.=	2.33.33
11° 40′= " " "	543+	E. C.=sta.	543+86.86
	86.86		

100—53.53=46.47×3′(def. for 1 ft. of 10° Cur.)=139.41′=
2° 19½″=def. for sta. 542.

Def. for 50 ft.=2° 30′ for a 10° Curve.

Def. for 36.86 ft.=1° 50½′ for a 10° Curve

(These tables are published in Field Books of
KEUFFEL & ESSER Co., New York, N. Y.)



PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 24 FEET WIDE. SIDE SLOPES 1½ to 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.
R.